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# Elasticity of Grossular-Andradite Solid Solution: An Ab initio Investigation. 

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$A b$ initio simulations of the elastic properties of the silicate garnet grossular-andradite solid solution, $\mathrm{Ca}_{3} \mathrm{Fe}_{2-2 x} \mathrm{Al}_{2 x}\left(\mathrm{SiO}_{4}\right)_{3}$, are performed, using an all-electron local basis set of Gaussian-type orbitals and the hybrid B3LYP density functional. The dependence of the bulk modulus (obtained by fitting energyvolume data to an equation-of-state) on composition $x$ is investigated over the whole range $0 \leq x \leq 1$. The bulk modulus is also computed following an independent approach, from elastic tensor calculations: results almost coincide with those of the equation-of-state scheme, thus confirming the high numerical accuracy of all the adopted algorithms. Contrary to what previously conjectured from a number of "heterogeneous" experimental measurements, a rather linear trend is predicted for the bulk modulus as a function of $x$, up to 20 GPa . The largest deviation from linearity is about 0.5 GPa at ambient conditions; it progressively reduces to less than 0.2 GPa at $P=20 \mathrm{GPa}$.

## I. INTRODUCTION

The characterization of the deep structure of the Earth is essentially based on seismic surveys and relies on the knowledge of the elastic properties of its individual constituents. Silicate garnets are among the most important rock-forming minerals of the upper mantle and transition zone, between 400 km and 670 km depth. ${ }^{78}$

Different compositional models of the mantle have been proposed, starting from the known elastic behavior of various minerals. In particular, Anderson and Bass ${ }^{79,80}$ have proposed a chemically heterogeneous model according to which the transition region is richer in calcium than the upper mantle, containing Ca-bearing silicate garnets, such as grossular, $\mathrm{Ca}_{3} \mathrm{Al}_{2}\left(\mathrm{SiO}_{4}\right)_{3}$, and andradite, $\mathrm{Ca}_{3} \mathrm{Fe}_{2}\left(\mathrm{SiO}_{4}\right)_{3}$. At geophysical conditions, grossular and andradite naturally occur as a solid solution, grandite $\mathrm{Ca}_{3} \mathrm{Fe}_{2-2 x} \mathrm{Al}_{2 x}\left(\mathrm{SiO}_{4}\right)_{3}$, displaying a range of compositions $x$ on which its elastic properties certainly depend. By combining the few available experimental bulk moduli of grandite solid solutions, ${ }^{81-83}$ a significant deviation from linearity seems to turn out, as discussed by O'Neill et al., ${ }^{83}$ at variance with the linear composition-modulus trend observed for the pyrope-almandine-spessartine (pyralspite) series, $(\mathrm{Mg}, \mathrm{Fe}, \mathrm{Mn})_{3} \mathrm{Al}_{2} \mathrm{Si}_{3} \mathrm{O}_{12}$. However, uncertainty and nonhomogeneity of the measurements still leave room for further insights.

Some of the present authors have recently demonstrated that $a b$ initio simulations do represent an effective and reliable tool for investigating the elastic properties

[^0](elastic constants, bulk, shear and Young moduli, directional seismic wave velocities, elastic anisotropy index, Poisson's ratio, etc.) of the end-members of this class of materials at ambient pressure ${ }^{84,85}$ and at geophysical pressures up to $60 \mathrm{GPa},{ }^{86}$ by comparing with available experimental data. ${ }^{87-102}$ Assuming a linear transferability of the computed $a b$ initio elastic properties from end-members to solid solutions also provided accurate estimates for a set of 32 solid solutions of pyralspite, ${ }^{96}$ whose end-members have bulk moduli relatively close to one another. ${ }^{87,93,103}$ The grandite solid solution appears as a more complex system where relatively large deviations from linearity of its bulk modulus as a function of chemical composition have been experimentally reported. As a consequence, the sole theoretical characterization of the elastic properties of the two end-members seems not enough, in this case. An explicit treatment of the compositional effect on its bulk modulus is required.

In this paper we undertake an explicit $a b$ initio theoretical study of the elastic properties of the grandite solid solution, $\mathrm{Ca}_{3} \mathrm{Fe}_{2-2 x} \mathrm{Al}_{2 x}\left(\mathrm{SiO}_{4}\right)_{3}$, as a function of its composition $x$. A structural model which refers to the 8 available sites for substitution in the end-member primitive cell is adopted. The whole composition range, $0 \leq x \leq 1$, is investigated; in particular, apart from the two end-members, other seven intermediate compositions are considered $(x=0.125,0.25,0.375,0.5,0.625$, 0.75 and 0.875 ). Each intermediate composition is represented by a number of independent atomic configurations efficiently selected through a symmetry-adapted sampling of the configuration space ${ }^{104}$ recently developed by Mustapha et al. ${ }^{105}$ and D'Arco et al. ${ }^{106}$

Calculations are performed with the Crystal14 program for $a b$ initio quantum chemistry and physics of the solid state, ${ }^{104,107}$ which features a general, fully au-
tomated procedure for computing elastic properties of periodic systems of any symmetry. ${ }^{84,108}$ The fully periodic implementation of the hybrid B3LYP ${ }^{109,110}$ functional and all-electron Gaussian basis sets are used. The same computational approach has already been successfully applied to the investigation of structural, electronic, vibrational (Infrared and Raman), magnetic and optical properties of silicate garnets. ${ }^{111-117}$

The structure of the paper is as follows: Section II illustrates the theoretical methodology adopted for the determination of the equation of state (EOS), the calculation of the bulk modulus via elastic constants and the definition of a structural model of the solid solution; computational parameters are given in Section III; calculated bulk moduli are discussed in Section IV; conclusions are drawn in Section V.

## II. THEORETICAL METHOD

## A. Equations of State

An approach that is commonly adopted for computing the bulk modulus of a crystalline material is via socalled Equations of State (EOS). A "cold" EOS is an energy-volume (or pressure-volume) relation which describes the behavior of a solid under compression and expansion, at $T=0 \mathrm{~K}$, that is the case of standard $a b$ initio simulations. Universal, i.e. not specific of particular materials, EOS are usually expressed as analytical functions of a limited set of parameters (equilibrium energy $E_{0}$, equilibrium volume $V_{0}$, equilibrium bulk modulus $K_{0}=-V \partial P / \partial V$ and pressure derivative of equilibrium bulk modulus $K_{0}^{\prime}=\partial K_{0} / \partial P$ ) for ease of interpolation, extrapolation and differentiation, and are quite used in solid state physics and geophysics. ${ }^{18,119}$

Energy-volume data are numerically fitted to the analytical $E(V)$ functional form of the EOS. From $P=$ $-\partial E / \partial V$, the $P-V$ connection is established. In principle, an advantage of this approach would be the possibility of predicting the high-pressure behavior of a solid from low-pressure or even equilibrium properties: the explicit dependence of the bulk modulus on volume (or pressure from $P-V$ ), is then given by $K(V)=$ $V \partial^{2} E / \partial V^{2}$.

A number of universal EOS have been proposed so far. ${ }^{18,120-125}$ All of them are phenomenological and can behave quite differently from each other as regards extrapolation at high pressure. Comprehensive reviews and comparisons of different EOS are available in the literature. ${ }^{126-130}$ Four EOS are currently implemented in the Crystal14 program: the original thirdorder Murnaghan's, ${ }^{120}$ the third-order Birch's, ${ }^{121,122}$ the logarithmic Poirier-Tarantola's, ${ }^{125}$ and the exponential Vinet's. ${ }^{123}$

## B. Elastic Constants and Related Properties

The elements of the fourth-rank elastic tensor $\mathbf{C}$ for 3D systems are usually defined as second energy density derivatives with respect to pairs of deformations: ${ }^{131}$

$$
\begin{equation*}
C_{v u}=\left.\frac{1}{V} \frac{\partial^{2} E}{\partial \eta_{v} \partial \eta_{u}}\right|_{0} \tag{1}
\end{equation*}
$$

where $\boldsymbol{\eta}$ is the symmetric second-rank pure strain tensor and Voigt's notation is used according to which $v, u=1, \ldots, 6(1=x x, 2=y y, 3=z z, 4=y z, 5=$ $x z, 6=x y)$. The elastic $\mathbf{C}$ tensor exhibits, in general, 21 independent elements that reduce to 3 (i.e. $C_{11}, C_{12}$ and $C_{44}$ ) for crystals with cubic symmetry, as in the case of silicate garnet end-members. Tensor $\mathbf{S} \equiv \mathbf{C}^{-1}$ is the socalled compliance tensor. A fully-automated and general procedure for computing elastic tensors under pressure, photoelastic constants and seismic velocities of crystals of any symmetry has recently been implemented in the Crystal program. ${ }^{84,86,132-138}$
Elastic properties of isotropic polycrystalline aggregates can be computed from the elastic and compliance constants defined above via the Voigt-Reuss-Hill averaging scheme. ${ }^{139}$ For crystals of any symmetry, an average bulk modulus $\bar{K}=1 / 2\left[K_{V}+K_{R}\right]$ can be defined between Voigt upper bound

$$
K_{V}=\frac{1}{9}\left[C_{11}+C_{22}+C_{33}+2\left(C_{12}+C_{13}+C_{23}\right)\right]
$$

and Reuss lower bound

$$
K_{R}=\left[S_{11}+S_{22}+S_{33}+2\left(S_{12}+S_{13}+S_{23}\right)\right]^{-1}
$$

For cubic crystals, these two bounds coincide and the bulk modulus $\bar{K}$ simply reduces to:

$$
\begin{equation*}
\bar{K}=\frac{1}{3}\left(C_{11}+2 C_{12}\right) . \tag{2}
\end{equation*}
$$

## C. Structural Model for Solid Solution

Reference is made to the primitive unit cell of the end-members (cubic space group $\mathcal{G} \equiv I a \overline{3} d$ ), which counts $|\mathcal{G}|=48$ symmetry operators and 4 formula units $\mathrm{Ca}_{3} \mathrm{Y}_{2}\left(\mathrm{SiO}_{4}\right)_{3}$. The structure displays dodecahedral (Ca), tetrahedral (Si) and octahedral (Y) crystallographic sites. There are 8 Y sites involved for substitutions. Solid solutions are obtained from andradite by progressively replacing $\mathrm{Fe}^{3+}$ with $\mathrm{Al}^{3+}$ cations. Apart from the two end-members, andradite $(x=0)$ and grossular ( $x=1$ ), other seven compositions are explicitly considered: $x=0.125,0.25,0.375,0.5,0.625,0.75$ and 0.875 .
For each composition $x, n_{\mathrm{Al}}=8 x$ aluminum atoms are present that correspond to $8!/\left[n_{\mathrm{Al}}!\left(8-n_{\mathrm{Al}}\right)!\right]$ different substitutional configurations, i.e. cation distributions among the Y sites. Altogether, the configurations sum up
to 256 over the whole range of compositions. Following the symmetry analysis recently proposed by Mustapha et al., ${ }^{105}$ these configurations can be partitioned into 23 distinct symmetry independent classes (SIC). Each class $L$ consists of $\mathcal{M}_{L} \equiv \mathcal{M}_{l}^{x}=|\mathcal{G}| /\left|\mathcal{H}_{L}\right|$ configurations that belong to a symmetry subgroup of order $\left|\mathcal{H}_{L}\right|$ of the aristotype symmetry, where $l$ is a relative index of the classes within a given composition $x$.

Since all the configurations of a given SIC are equivalent to each other, the number of calculations to be actually performed reduces to one per SIC, that is, to a total of $23 . \mathcal{M}_{L}$ can then be interpreted as the multiplicity of class $L$. Only the highest spin ferromagnetic configurations will be considered, as the difference between ferromagnetic and anti-ferromagnetic energies was shown to be extremely small. ${ }^{140}$
A list of all the configurations studied, along with their symmetry and multiplicity, is given in Table I. The two end-members are described by a single cubic class with $\mathcal{M}_{L}=1$. Compositions $x=0.125$ and $x=0.875$ can be described by a single trigonal class ( $L=2$ and $L=$ 22 , respectively) with $\mathcal{M}_{L}=8$ equivalent atomic configurations. For describing compositions $x=0.25$ and $x=$ 0.75 , three classes are required, one of trigonal symmetry with a multiplicity of 4 and two of monoclinic symmetry with a multiplicity of 12 . Three classes are also required for modeling the $x=0.375$ and $x=0.625$ compositions: one trigonal and two triclinic with multiplicities of 8 and 24 , respectively. The middle composition $x=0.5$ is represented by seven classes: one cubic, one orthorhombic, one tetragonal, one trigonal, two monoclinic, and one triclinic, which, in Table I, are sorted in terms of decreasing symmetry and increasing multiplicity.

## III. COMPUTATIONAL DETAILS

Calculations are performed with the Crystal14 program. ${ }^{104}$ The B3LYP one-electron Hamiltonian is adopted, which contains a hybrid Hartree-Fock/DensityFunctional exchange-correlation term. The valence openshell of $\mathrm{Fe}^{3+}\left(d^{5}\right)$ requires a spin-polarized solution. Allelectron atom-centered Gaussian-type-function (GTF) basis sets are adopted. Oxygen, silicon, aluminum and calcium atoms are described in order by ( $8 s$ )$(411 s p)-(1 d),(8 s)-(6311 s p)-(1 d),(8 s)-(611 s p)-(1 d)$ and $(8 s)-(6511 s p)-(21 d)$ contractions of primitive GTFs. For iron, a $(8 s)-(64111 s p)-(411 d)$ contraction of GTFs is used, augmented with a further $f$-type polarization function as reported into details in previous works. ${ }^{112,113,141}$

In Crystal, the truncation of infinite lattice sums is controlled by five thresholds, which are set to $7,7,7,8$, 16. ${ }^{107}$ Reciprocal space is sampled according to a sublattice with shrinking factor 2 , which corresponds to a number of irreducible $\mathbf{k}$-points in the first Brillouin zone between 3 and 8 , depending on the symmetry of the configuration. The DFT exchange-correlation contribution is evaluated by numerical integration over the cell vol-

TABLE I. The 23 symmetry independent classes of atomic configurations used to model the grandite solid solution at nine compositions $x$ are listed and labeled with the absolute index $L$ and a relative index $l$ within each composition. The symmetry of the corresponding lattice and multiplicity of each class are also reported.

|  |  |  |  |  |
| :--- | ---: | :--- | :--- | ---: |
| $x$ | $L$ | $l$ | Lattice | $\mathcal{M}_{L} \equiv \mathcal{M}_{l}^{x}$ |
|  |  |  | Cubic | 1 |
| 0.125 | 1 | 1 | Cubic | 8 |
|  | 3 | 1 | Trigonal | 4 |
| 0.25 | 4 | 2 | Trigonal | Monoclinic |

ume: radial and angular points of the atomic grid are generated through Gauss-Legendre and Lebedev quadrature schemes, using an accurate predefined pruned grid (keyword XLGRID). The convergence threshold on energy for the self-consistent-field (SCF) step of the calculations is set to $10^{-9}$ hartree.

Equilibrium and strained configurations are optimized calculating analytical energy gradients with respect to both atomic coordinates and unit-cell parameters or atomic coordinates only. ${ }^{142-144}$ A quasi-Newtonian technique is used, combined with the BFGS algorithm for Hessian updating. ${ }^{145-148}$ Convergence is checked on both gradient components and nuclear displacements; the corresponding tolerances on their root mean square are chosen to be 10 times more severe than the default values for simple optimizations: 0.00003 a.u. and 0.00012 a.u., respectively.
As regards EOS calculations, five hydrostatic compressions (up to $14 \%$ in volume) and five hydrostatic expansions (up to $8 \%$ in volume) are applied to each configuration and a constant-volume optimization is performed at each step. Energy-volume data are then fitted to a thirdorder Birch-Murnaghan EOS ${ }^{121,122}$ for the determination of the corresponding bulk modulus, $K_{\text {EOS }}$.

For the elastic constants calculation, two strained
configurations are considered for each symmetryindependent strain (two for cubic and six for triclinic crystals), with a dimensionless strain amplitude of 0.01 .

## IV. RESULTS AND DISCUSSION

Before illustrating our theoretical results on the elastic behavior of the grossular-andradite solid solution series, let us summarize the main findings of previous studies. In Figure 1, we collect the outcomes of experimental measurements on the evolution of the bulk modulus $K$ of grandite as a function of composition $x$. Available experimental data are represented by solid symbols. ${ }^{81,82,149-153}$

Two values are reported at $x \approx 1$, which represent the grossular end-member (natural single crystal samples pure to $97 \%$ and $99 \%$, respectively): an ultrasonic measurement by Halleck ${ }^{149}$ (triangle) provided $K=$ $171.4 \pm 1.7 \mathrm{GPa}$, and a Brillouin scattering experiment performed by Bass ${ }^{151}$ (square) yielded $K=168.4 \pm 0.7$ GPa. As regards andradite, two values are reported as determined by Brillouin spectroscopy: $K=157 \pm 2 \mathrm{GPa}$ by Bass ${ }^{82}$ (circle) and $K=154.5 \pm 0.6$ GPa by Jiang et al. ${ }^{153}$ (inverted triangle). Let us stress that, even for the two end-members, different experimental determinations of their bulk moduli can hardly be considered compatible with each other on the grounds of the corresponding uncertainties (see the error bars reported in Figure 1). Experimental uncertainties become even larger for most of the intermediate compositions, as we shall discuss below.
The main experimental investigation of the elastic properties of intermediate compositions of the grandite solid solution has been performed by Babuska et al. in $1978^{81}$ by means of the rectangular parallelepiped resonance method. They analyzed four specimens of three different composition: $\mathrm{Gr}_{79.9} \mathrm{An}_{14.2}, \mathrm{Gr}_{76.1} \mathrm{An}_{22.1}$, and $\mathrm{An}_{70.4} \mathrm{Gr}_{22.2}$. The corresponding bulk moduli are represented as rhombi in Figure 1. The three grossularrich samples provide $K$ in the range $161-164 \mathrm{GPa}$. The andradite-rich sample showed a bulk modulus of $147.3 \pm$ 3.4 GPa. More recently, in 2004, Jiang et al. ${ }^{152}$ performed Brillouin spectroscopy on a grossular-rich garnet of composition $\mathrm{Gr}_{87} \mathrm{An}_{9} \mathrm{Py}_{2} \mathrm{Al}_{2}$ (Py stands for pyrope, Al for almandine), for which they obtained $K=165.8 \pm 0.5$ GPa (pentagon).

The dashed line in Figure 1 represents the bulk modulus trend as a function of composition $x$ which was proposed by O'Neill et al. ${ }^{83}$ in 1989, on the grounds of available experimental data at that time. Nowadays, having at hand also more recent determinations of $K$, we can see how the proposed pronounced deviation from linearity is mainly dominated by the sole value at about $x=$ 0.22 . The solid line in the figure represents our theoretical results, to be discussed into detail in what follows, which clearly shows a quasi-linear behavior of the elastic response of the grandite solid solution as a function of its chemical composition.


FIG. 1. Variation of the bulk modulus $K$ of the grandite solid solution $\mathrm{Ca}_{3} \mathrm{Fe}_{2-2 x} \mathrm{Al}_{2 x}\left(\mathrm{SiO}_{4}\right)_{3}$ as a function of composition $x$. The solid line shows the quasi-linear trend of our calculated values, whereas the dashed curve is drawn to provide an approximate fit to the experimental data, as suggested by O'Neill et al. ${ }^{83}$ Experimental data are from Halleck ${ }^{149}$ ( $\mathrm{Gr}_{97.4}$, triangle), Babuska et al. ${ }^{81}$ (intermediate compositions, rhombi), $\mathrm{Bass}^{82}\left(\mathrm{An}_{96} \mathrm{Gr}_{3.7} \mathrm{Py}_{0.3}\right.$, circle), Bass ${ }^{151}$ ( $\mathrm{Gr}_{99.2}$, square), Jiang et al. ${ }^{152}$ ( $\mathrm{Gr}_{87} \mathrm{An}_{9} \mathrm{Py}_{2} \mathrm{Al}_{2}$, pentagon) and Jiang et al. ${ }^{153}\left(\mathrm{Gr}_{2} \mathrm{An}_{98}\right.$, triangle). Here, Gr stands for grossular, An for andradite, Py for pyrope, and Al for almandine. When available, error bars are also shown.

For each composition $x$ and each symmetry independent class, we have computed the equation of state of a representative atomic configuration, according to the procedure described in Section III. The calculated bulk moduli $K_{\text {EOS }}$ are reported in Table II. As regards the two end-members, computed values are found to be in agreement with experimental data within $1 \%$ for grossular and $3 \%$ for andradite.

The numerical accuracy of the EOS determinations of the bulk moduli is checked by comparison with the analytical bulk moduli $K_{V}, K_{R}$ and $\bar{K}$ calculated from the elastic tensor $\mathbf{C}$ of equation (1), according to Voigt-Reuss-Hill averaging scheme. These three elastic determinations of the bulk modulus are also reported in Table II. The following considerations can be made: i) the agreement between $\bar{K}$ and $K_{\text {EOS }}$ is excellent (within 0.9 $\%$ ) in the whole composition range, which confirms the extremely high numerical accuracy of all the algorithms involved; ii) the values of $K_{\mathrm{EOS}}$ obtained for polymorphic classes are very close to one another, with differences never larger than $0.1 \%$; iii) $K_{V}$ and $K_{R}$ essentially coincide with each other within any class, regardless of the

TABLE II. For each symmetry independent class, labeled by the absolute index $L$ and relative index $l$ within each composition $x$, the bulk modulus $K(\mathrm{GPa})$ is reported as computed with an EOS approach, $K_{\text {EOS }}$, and from the elastic constants following Voigt's, $K_{V}$, Reuss's, $K_{R}$, and Hill's, $\bar{K}$, prescriptions. $\Delta E=E_{l}^{x}-E_{\text {min }}^{x}($ in mHa$)$ is the difference between the energy of configuration $l$ at composition $x, E_{l}^{x}$, and the energy of the most stable configuration with the same composition, $E_{\text {min }}^{x} \cdot{ }^{a}$

|  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $x$ | $L$ | $l$ | $\Delta E$ | $K_{\text {EOS }}$ | $K_{V}$ | $K_{R}$ | $\bar{K}$ |
| 0. | 1 | 1 | - | 150.0 | 149.7 | 149.7 | 149.7 |
| 0.125 | 2 | 1 | - | 151.9 | 150.8 | 150.8 | 150.8 |
| 0.25 | 3 | 1 | 2.335 | 153.9 | 153.6 | 153.6 | 153.6 |
|  | 4 | 2 | 1.634 | 154.0 | 153.2 | 153.2 | 153.2 |
|  | 5 | 3 | - | 153.9 | 153.8 | 153.8 | 153.8 |
| 0.375 | 6 | 1 | 3.002 | 156.0 | 156.3 | 156.3 | 156.3 |
|  | 7 | 2 | 1.721 | 156.0 | 154.6 | 154.6 | 154.6 |
|  | 8 | 3 | - | 156.0 | 155.1 | 155.1 | 155.1 |
|  | 9 | 1 | 5.925 | 158.3 | 157.8 | 157.8 | 157.8 |
|  | 10 | 2 | 3.053 | 158.1 | 157.4 | 157.4 | 157.4 |
|  | 11 | 3 | - | 158.1 | 157.6 | 157.6 | 157.6 |
| 0.5 | 12 | 4 | 1.267 | 158.2 | 157.2 | 157.2 | 157.2 |
|  | 13 | 5 | 1.541 | 158.1 | 158.2 | 158.1 | 158.2 |
|  | 14 | 6 | 1.946 | 158.1 | 158.0 | 157.9 | 158.0 |
|  | 15 | 7 | 3.289 | 158.2 | 157.3 | 157.3 | 157.3 |
|  | 16 | 1 | 3.259 | 160.3 | 160.1 | 160.1 | 160.1 |
| 0.625 | 17 | 2 | 1.382 | 160.3 | 160.2 | 160.2 | 160.2 |
|  | 18 | 3 | - | 160.3 | 159.3 | 159.3 | 159.3 |
|  | 19 | 1 | 2.131 | 162.4 | 162.6 | 162.6 | 162.6 |
| 0.75 | 20 | 2 | 1.954 | 162.6 | 162.5 | 162.5 | 162.5 |
|  | 21 | 3 | - | 162.6 | 161.8 | 161.7 | 161.8 |
| 0.875 | 22 | 1 | - | 164.9 | 163.9 | 163.9 | 163.9 |
| 1. | 23 | 1 | - | 167.3 | 167.1 | 167.1 | 167.1 |

[^1]specific symmetry of the corresponding lattice. Since $K_{V}$ and $K_{R}$ are expected to coincide only for cubic systems, their equality appears consistent with the pseudo-cubic metric attributed to grandite solid solutions by both experimental and theoretical investigations. Details about the minimum energy structures of the different classes, as obtained with B3LYP geometry optimizations, are reported in Ref. 154. All the calculated cells are pseudocubic, with the three lattice parameters differing from each other by less than $0.01 \AA$, and angles that deviate by less than $0.4^{\circ}$ from right angles.

A Boltzmann average bulk modulus, $K_{a v}^{x}$, may be defined for any composition $x$ :

$$
\begin{equation*}
K_{a v}^{x}=\sum_{l} \mathcal{P}_{l}^{x} K_{l}^{x} \tag{3}
\end{equation*}
$$



FIG. 2. Deviation from linearity ( $\Delta K$ in GPa) of the Boltzmann average bulk modulus of grandite, calculated via the EOS approach, as a function of chemical composition $x$ and pressure. Temperature $T$ is fixed at 298 K .
where

$$
\begin{equation*}
\mathcal{P}_{l}^{x}=\frac{\mathcal{M}_{l}^{x} \exp \left(-\frac{\Delta E_{l}^{x}}{k_{B} T}\right)}{\sum_{l} \mathcal{M}_{l}^{x} \exp \left(-\frac{\Delta E_{l}^{x}}{k_{B} T}\right)} \tag{4}
\end{equation*}
$$

is the probability of finding the $l$-th class of composition $x$ at temperature $T$. In the expression above, $\Delta E_{l}^{x}=E_{l}^{x}-$ $E_{\min }^{x}$ is the difference between the energy of configuration $l$ at composition $x$ and the energy of the most stable configuration with the same chemical composition. These energy differences are reported in Table II, along with the energies of the most stable configurations per each composition $x$.

The average bulk moduli for all the considered compositions $x$ have been computed at $T=298 \mathrm{~K}$ via equations (3) and (4), and reported, as a continuous line, in Figure 1 where they are compared with the available experimental data discussed at the beginning of this section. On the scale of that figure, as anticipated before, computed values show an almost linear behavior as a function of the chemical composition of the grandite solid solution.

A closer look at the computed data reveals that the dependence of the grandite bulk modulus on chemical composition is not perfectly linear. In Figure 2, we report the deviation from linearity of the average bulk modulus, $\Delta K_{a v}$, as a function of $x$. At zero pressure, a maximum deviation of about -0.5 GPa is observed at $x=0.5$.

The EOS approach that we have followed allows to compute the bulk modulus also under increasing hydrostatic pressure. In this respect, an EOS could be used
in two quite different modes: i) to extrapolate at high pressure from small compression data or ii) to interpolate from large compression data. As we recently discussed, ${ }^{86}$ mode $i$ ) is extremely sensitive to the particular analytical expression adopted for the EOS whereas mode ii) is almost independent of the specific expression of the EOS. In this study we use the latter approach by explicitly computing the energy of each configuration up to volume compressions of $14 \%$, which roughly correspond to $P=25 \mathrm{GPa}$. The deviation from linearity of the bulk modulus, as evaluated at about $7 \mathrm{GPa}, 15 \mathrm{GPa}$ and 20 GPa , is shown in the figure. It can be seen that the maximum deviation decreases as a function of pressure from about -0.5 GPa at zero pressure to about -0.35 GPa at $7 \mathrm{GPa},-0.23 \mathrm{GPa}$ at 15 GPa and -0.15 GPa at 20 GPa of pressure. Within the explored pressure interval, the deviation from linearity of the bulk modulus decreases as pressure increases.

## v. CONCLUDING REMARKS

Periodic B3LYP quantum-chemical simulations have been performed on the elastic properties of the grandite solid solution, $\mathrm{Ca}_{3} \mathrm{Fe}_{2-2 x} \mathrm{Al}_{2 x}\left(\mathrm{SiO}_{4}\right)_{3}$, at various compositions $x$ in the whole range $0 \leq x \leq 1$. The bulk modulus of 23 symmetry-independent atomic configurations has been computed following two independent approaches: from the elastic tensor and from fitting energy-volume data to the Birch-Murnaghan equation-of-state. Discrepancies between the two schemes are negligible, thus demonstrating high numerical accuracy and consistency of the algorithms involved.

While "heterogeneous" experimental measurements were suggesting a pronounced non-linear trend of the bulk modulus of the solid solution as a function of its chemical composition (with a maximum deviation of about 7 GPa ), the present theoretical results reveal a quasi-linear behavior. A slight deviation from linearity is reported at low pressure, with a maximum value of 0.5 GPa , which is then further reduced under increasing pressure, up to 20 GPa .

The present findings contribute to the definition of a homogeneous frame according to which all the solid solutions of the most abundant silicate garnets (pyralspite and grandite) exhibit linear elastic properties as a function of their chemical composition. Linearity of pyralspite is well-known since long whereas the presumed nonlinearity of the grandite system has been here demonstrated to be an artifact of heterogeneous experimental measurements.

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[^1]:    ${ }^{\bar{a}} E_{\text {min }}^{0.0}=-25329.246886 \mathrm{Ha}, E_{\text {min }}^{0.125}=-24308.149454 \mathrm{Ha}$,
    $E_{\min }^{0.25}=-23287.054557 \mathrm{Ha}, E_{\min }^{0.5}=-22265.958966 \mathrm{Ha}$,
    $E_{\min }^{0.375}=-21244.865171 \mathrm{Ha}, E_{\min }^{0.625}=-20223.769247 \mathrm{Ha}$,
    $E_{\min }^{0.75}=-19202.676027 \mathrm{Ha}, E_{\min }^{0.875}=-18181.582403 \mathrm{Ha}$,
    $E_{\text {min }}^{1.0}=-17160.490459 \mathrm{Ha}$

