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(Article begins on next page)

1 **GPR surveys for the prevention of karst risk in underground gypsum quarries.**

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11

12 Abstract

13 The investigation and prediction of geological anomalies in underground quarries is fundamental to
14 ensure safety, efficiency and economic convenience of the exploitation. For these aims, non-
15 destructive geophysical surveys may be an effective alternative approach to classical destructive
16 prospecting techniques (i.e. horizontal drilling), with great advantages particularly in complex
17 geological frameworks and in areas subjected to specific geo-hazards. Ground Penetrating Radar
18 (GPR), for its high resolution, is a suitable technique for underground excavations, particularly for
19 the identification of water bodies, fissures and fractured rocks. The present study is focused on the
20 application of GPR for the prediction of karst structures in underground gypsum quarries. Karst
21 phenomenon is a main risk factor for gypsum orebodies, where large cavities may be intersected by
22 the excavation. The possible filling with clay or pressurized water of these cavities exponentially
23 increases the dangerousness of the phenomenon, due to swelling problems and violent water inrushes.
24 The aim of the present study is to propose, through modelling and field surveys, a description of GPR
25 outputs for principal elements of karst hazard in gypsum bodies, with particular attention to the
26 discrimination of fillings (air, water or clay).

27

28 **Keywords:** GPR, Gypsum, Karst, Underground exploitation

29

1. Introduction

In underground mining activities several geological problems can interfere with excavation safety, environmental sustainability and the general efficiency in the exploitation of resources.

The mining site safety can be endangered, *in primis*, by mechanical and structural features of the rock mass. In this framework, for instance, structural weaknesses may cause the split-up of instable blocks, with generation of collapses, or may decrease the stability of the underground drifts, by damaging support elements such as pillars or walls. These weaknesses usually manifest with ongoing fracturing at the excavation front or within the rock mass. In gypsum orebodies, other problems, due to the presence of karst phenomena and pressurized water in fractures or caves, can arise. Violent water inrushes connected with karst phenomenon may cause serious consequences in both environmental and safety fields. Several research groups dealt with tunnel instability induced by large-scale karst phenomenon, trying to determinate the minimum safety thickness of tunnel rock walls for resisting water inrushes (e.g. Jiang et al., 2017; Xu et al., 2018; Wu et al., 2019). The possibility to forecast the presence of karst voids and to understand the nature of filling materials (air, water or clay) has therefore a relevant interest. The use of indirect geophysical methods offers some advantages in terms of repeatability and rapidity, representing an alternative method to classical destructive prospecting techniques (i.e. horizontal drilling).

Among geophysical methods, Ground Penetrating Radar (GPR) is an electromagnetic technique primarily designed for location of objects or interfaces buried beneath the earth's surface or located within a visually opaque structure (Daniels, 2004). The application of this technique is based on the propagation and reflection of a high frequency (10 MHz – 2.5 GHz) electromagnetic signal. GPR has been used since mid 90s for applications in civil engineering, but it is with the technological advancements and tremendous improvements of digital computation power in the last decades that GPR applications had a blossoming. Several application fields can be remembered including geotechnical applications (Wai-Lok Lai et al., 2018).

1 An important application field of GPR is the localization of water content zones (Afshar et al., 2015;
2 Bowling et al., 2005; Mahmoudzadeh et al., 2012) and of morphologies connected to karst
3 phenomena, such as cavities and buried sinkholes (Afshar et al., 2015; Gómez-Ortiz and Martín-
4 Crespo, 2012; Pueyo-Anchuela et al., 2015; Sevil et al., 2017). Pueyo-Anchuela et al. 2009 codified
5 the GPR key-features of some karst-connected morphologies (i.e. sediment-filled cavities, evidences
6 of subsidence and paleo-collapses). They propose a “guide” to recognize these morphologies in GPR
7 profiles acquired from the surface, describing the expected geometrical relations among
8 electromagnetic reflectors (i.e. on-lap geometries, depressed reflectors, folded reflectors or laterally
9 abrupt changes of electromagnetic properties).

10 GPR method has been proposed and used for the assessment of fracturing and mechanical damage in
11 tunnel ahead prospecting, both in civil and mining frameworks, offering high resolution images about
12 the material behind the excavation face. Compared to seismic methods used for the same purposes,
13 GPR provides higher resolution data but lower penetration depth (Li et al., 2017). In particular, in
14 mining environments, both during the mining design and the mining exploitation, the detailed
15 knowledge of the rock mass produced by GPR can indeed be of primary utility. As an example, in
16 this context, GPR has been already used to detect the presence of fractures (e.g. Kovic, 2011; Porsani
17 et al., 2006) and to infer the presence of microcracks and to evaluate the rock mass quality (e.g.
18 Dérobert and Abraham, 2000; Orlando, 2003). Kadioglu, 2008 suggested to apply this methodology
19 to recognize layers with different geological features. Aldas et al., 2006 proposed a method to use
20 GPR to obtain the subsurface images of rock discontinuities in order to improve the design of the
21 blasting pattern.

22 The present study proposes the application of GPR to forecast karst morphologies and to discriminate
23 their fillings in underground gypsum quarries. The low primary porosity of gypsum and the possibility
24 to have fluid circulation connected with secondary permeability (due to fractures or discontinuities)
25 frequently bring to the formation of karst phenomena in this material. GPR techniques were applied

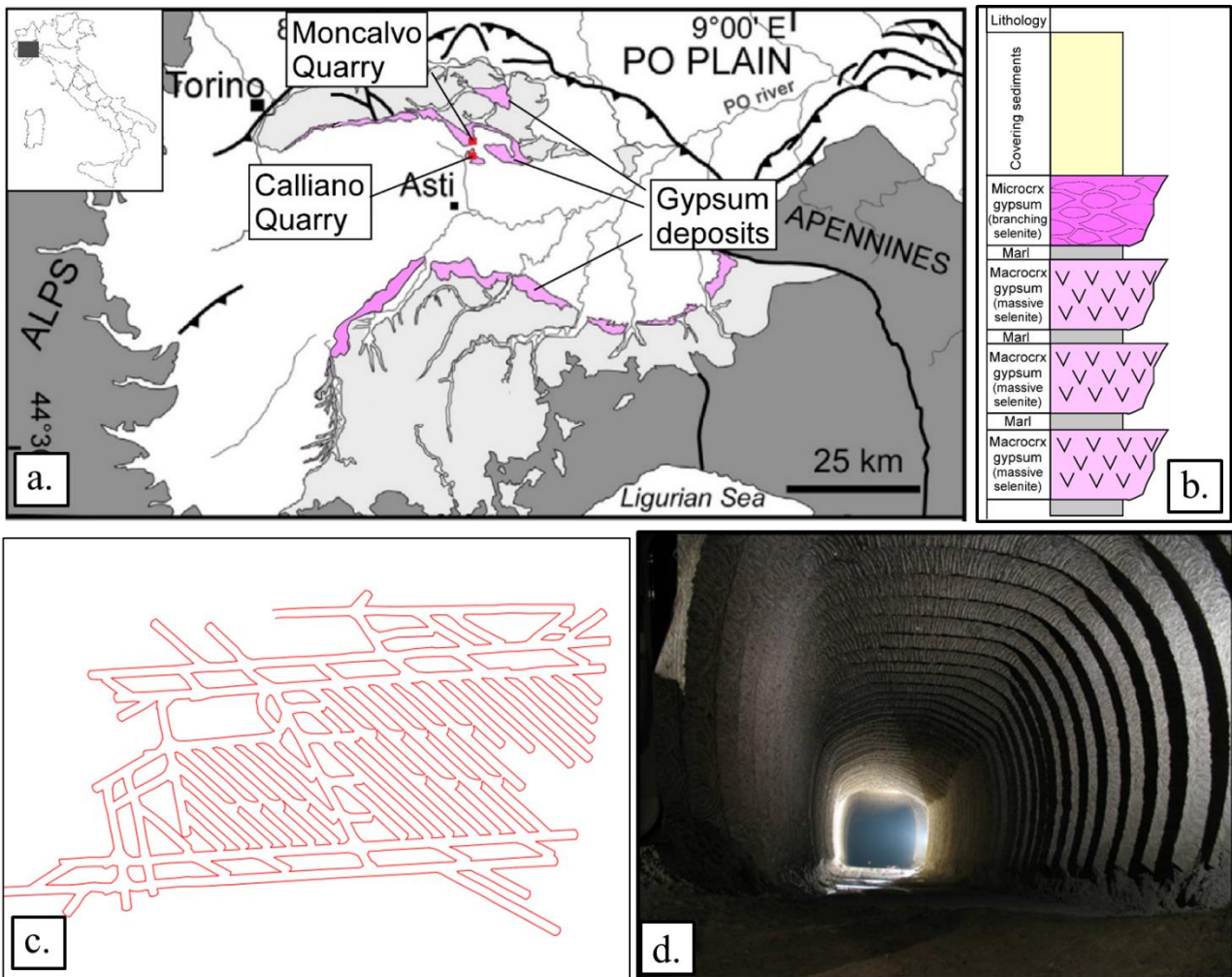
1 to the identification of the principal risk factors connected with karst phenomenon in underground
2 excavations and to the discrimination of filling materials (air, water or clay). Both modeled and
3 experimental data acquired in two test sites are hereafter presented.

4 2. Test sites: geological framework

5 The test sites are two gypsum quarries located in the Monferrato area (Piedmont, NW Italy):
6 Moncalvo quarry and Calliano quarry (Figure 1a). From a geological point of view, they are sited in
7 the Tertiary Piedmont Basin (TPB), a Late Eocene - Miocene complex sedimentary basin (Clari et
8 al., 1995; Piana and Polino, 1995). Gypsum beds are dated to Late Messinian age, when the so called
9 “Messinian Salinity Crisis” occurred (Dela Pierre et al., 2011). The stratigraphic characteristics of the
10 area see the gypsum unit sandwiched between marl and clayey sediments.

11 The quarries are exploited through underground excavations. The ore bodies consist of 4 gypsum
12 layers, each about ten meters thick, divided by marl layers a few meters thick (Figure 1b).
13 Stratigraphic discontinuities separating gypsum and marls layers dip to NW at low angle (10°-12°).
14 Going from bottom to top, there are 3 macrocrystalline gypsum layers (massive selenite gypsum) and
15 1 microcrystalline gypsum layer (branching selenite gypsum). Nowadays, the exploitation is active
16 in the first three layers from the top, while the macrocrystalline gypsum layer in the lower
17 stratigraphic position is not in use. The quarries are therefore organized in three underground levels.
18 The evaluation of mechanical properties for the stability assessment of the drifts is complicated by
19 the gypsum anisotropy and heterogeneity in compositional and textural features (Caselle et al. 2018,
20 Caselle et al. 2019a, Caselle et al. 2019b, Caselle et al. 2019c). The excavation works proceed using
21 continuous mining machinery, represented by a road header, because of gypsum low mechanical
22 resistance and abrasiveness and orebody regularity. The drifts do not intersect each other orthogonally
23 as in a blasting exploitation, but take a “lozenge pattern”, with a “rooms and rib pillars” exploitation
24 planning (Figure 1c) (Bonetto et al., 2008). The resulting excavation faces are smooth, with a regular
25 surface with average sizes of 6m x 6m, with rounded corners and a slight convexity. The advancement

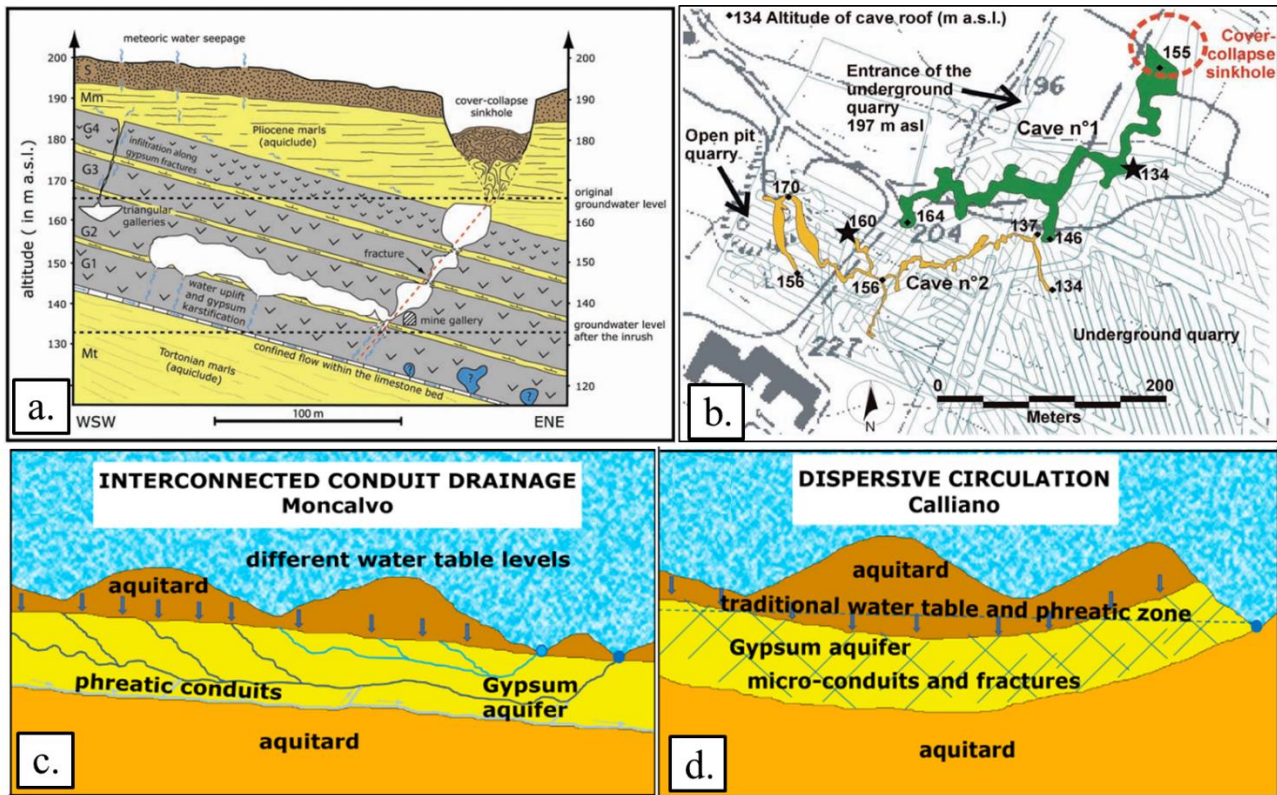
- 1 of the road header machine produces residual “waves” in the lateral walls of the drifts (Figure 1d).
- 2 Their amplitude (about 0.4 m) corresponds to the material exploited in each machine step.



3
 4 *Figure 1 a. Areal distribution of gypsum deposits in northwestern Italy and geographical localization of the test sites. b. Representative*
 5 *simplified stratigraphic column of the gypsum orebody. c. Lozenge drilling pattern for the excavation of gypsum with road header. d.*
 6 *Regular profile of the drilling drifts, with the “waves” produced by the machine advancement on the lateral walls.*

7 Evidences of karst phenomena were recognized in the gypsum layers of both quarries. The scheme
 8 in Figure 2a illustrates the principal features of the karst circulation in the area. The karst system is
 9 controlled by the presence of pre-existing fracturing (with a mean sub-vertical orientation) copulated
 10 with the sub-horizontal stratigraphic discontinuities, separating gypsum and marls. The permeability
 11 contrast of these stratigraphic discontinuities favours the water circulation within the gypsum body
 12 and the consequent dissolution processes, leading to the development of the karst conduits and

1 cavities. The presence of peculiar features makes, however, the two situations quite different, as
 2 described by Vigna et al., 2017 (Fig. 2c-d).



3
 4 *Figure 2 a. Scheme of the karst circuit characteristics in the gypsum body (Vigna et al. 2010; Bonetto et al., 2008) b. Moncalvo quarry*
 5 *map with the cartographical representation of the survived karst caves. The stars represent the points of intersection with the drifts*
 6 *(Vigna et al. 2010) c-d Conceptual models for karst circulation in gypsum (modified by Vigna et al., 2017):c. Interconnected conduit*
 7 *drainage karst system, recognized in Moncalvo quarry. d. Dispersive karst circulation system, recognized in Calliano quarry.*

8 In the Moncalvo quarry (Fig. 2c) the gypsum sequence is relatively compact. Both surficial waters
 9 and rising fluids, following sets of fractures in the upper and lower rocks (aquitards), recharge the
 10 karst circuits, creating an underground water circulation within conduits and caves. In this quarry, the
 11 karst problem assumed a particular relevance since 15th February 2005, when the incidental
 12 intersection of a karst circuit during mining works caused an inrush of 60,000 m³ of water mixed with
 13 mud causing the complete flooding of the lower quarry tunnels (Bonetto and Fornaro, 2005; Bonetto
 14 et al., 2008; Vigna et al., 2010). A big “camera” (a few hundred m³) was identified in contact with
 15 the level 1 drift where the inrush happened. From this “camera”, 850 meters of cave passages,
 16 characterized by typical phreatic morphologies, were observed (Fig. 2b). In this framework, the
 17 presence of karst conduits and karst caves is the principle cause of risk for the quarry activities. In

1 general, the dangerousness of these elements is determined by the filling. Particular attention is
2 therefore paid to the presence of clay or pressurized water. The monitoring activity has to be directed
3 mainly to the identification of karst caves shape and to the type of filling material.

4 A completely different hydrogeological situation can be found in Calliano quarry (Fig. 2d). Gypsum
5 beds are characterized by a much more intense fracturing, with numerous small karst conduits and
6 water-bearing fractures. Calliano is therefore a classical example of “dispersive karst circulation
7 system”, an extensively fractured and karstified aquifer with very good interconnection among
8 fractures and karst conduits. In this case, the monitoring activity has to be directed mainly to the
9 identification of small karst conduits and fractures, typically orientated vertically through the gypsum
10 beds, with particular attention to the possibility of a filling material (clay) or to the presence of
11 pressurized water.

12 3 Methodologies

13 Depending on the hydrogeological conditions and karst frameworks of gypsum orebodies, GPR
14 modelling and field surveys were directed to evaluate GPR potentialities in the identification of the
15 following elements:

- 16 - Karst conduits: despite their little diameters, they guarantee the alimentation of the karst
17 circuit and the connection among the different parts of the network. They are potentially
18 bearing large quantities of pressurized water;
- 19 - Karst cavities, with variable sizes from one to several cubic meters: their potential filling with
20 clay or water constitutes the principal source of danger for underground excavations;
- 21 - Open fractures: they are preferential ways for water circulation and represent structural
22 weaknesses for the rock-mass stability.

23 First, appropriate numerical models simulating the presence of all the above anomalies were
24 produced. Three different anomaly fillings (air, water, clay) were simulated to evaluate their influence

1 on the resulting radargrams and their possible identification. To confirm the evidences of numerical
2 models and to better evaluate the potentiality of GPR in the real quarry environment, field data were
3 acquired in different locations within the quarries where known anomalies were recognized.
4 Simulated and field radargrams were finally compared to allow for a combined evaluation of the GPR
5 potentiality in this environment.

6 3.1 Modelling

7 Numerical modeling of the three types of identified anomalies in the gypsum rock-mass were
8 developed and used to simulate the correspondent radar outputs. The code GprMax2D, based on a
9 finite-difference time-domain numerical method, was used for numerical simulations.

10 Numerical modelling was developed along 2d sections (oriented as shown in Figure 3a). The gypsum
11 orebody was simulated with appropriate electromagnetic features reflecting the average rock mass
12 properties. The possible anomalies were simulated adding to the rock-mass model geometrical entities
13 with the electromagnetic features of the desired filling (water, air or clay). Electromagnetic properties
14 of both the gypsum orebody and the investigated anomalies are reported in Table 1. These parameters
15 have been selected both on the analysis of experimental data and on the study of literature properties
16 for the investigated materials. The cell sizes in the models (Δx and Δy) were chosen in order to
17 minimize numerical dispersion, following

$$18 \quad \Delta x = \Delta y \leq \lambda/10 \quad \text{and}$$

$$19 \quad \Delta x = \Delta y < s/10$$

20 where λ is the wavelength of the signal and s is the size of the smallest modelled object. Considering
21 a central frequency of radar antenna of 200 MHz and the mean relative electrical permittivity of
22 gypsum (from Table 1), the expected wavelength is 0.45 m. The smallest modelled object (karst
23 conduit) has a diameter of 0.2 m. Therefore, cell sizes lower than 0.02 m allows for the respect both
24 the thresholds.

1 *Table 1 Relative electrical permittivity and electrical conductivity for the principal material involved in karst systems in gypsum beds.*

	Relative electrical permittivity [ϵ_r]	Electrical Conductivity [σ/m]
“Macrocrystalline” Gypsum	11	0.67×10^{-2}
“Microcrystalline” Gypsum	11	1.25×10^{-2}
Air	1	0
Water	80	0.25
Clay	8	2.5×10^{-2}

2

3 Over these constructed models, the GPR acquisition was simulated by passing the appropriate radar
 4 antenna (modelled as a line source) from the left to the right. Signal was simulated as a ricker wave,
 5 with central frequency of 200 MHz. Adsorbing Boundaries were included in the models at a certain
 6 distance from the investigated area (usually at least 15 cells) to avoid artificial reflections at model
 7 borders. Synthetic radargrams were therefore computed as the z-component of the electromagnetic
 8 field (perpendicular to the quarry face).

9 Synthetic radargrams were produced in a noise-free environment, to isolate and describe the GPR
 10 features of the potential targets in clear and well known conditions. This choice allows for a better
 11 description and classification of the GPR outputs. Moreover, the underground quarry environment is,
 12 in the overall, a quite noise free environment from the electromagnetic point of view. Performing the
 13 same synthetic simulations with the addition of a white noise to the synthetic data would be not
 14 particularly realistic. Eventual noise sources that could affect the real data are related to geological
 15 variability behind the excavation front and these are not easy to be simulated. Notwithstanding this
 16 eventual variability, under most of the simulated conditions, the correspondence of synthetic and real
 17 radargrams can be easily established, allowing for a combined evaluation of the GPR potentiality in
 18 the quarry environment.

19

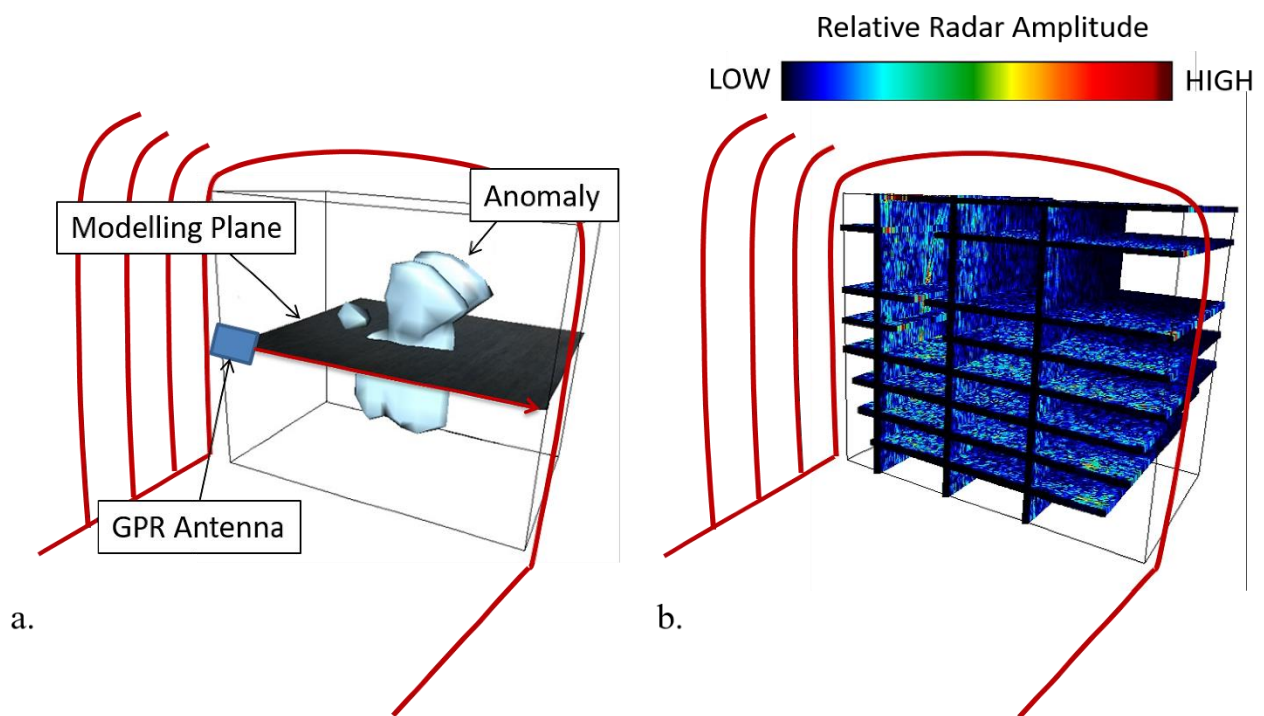
3.2 Field data acquisition and processing

Radar data were acquired on the excavation faces with a K2 IDS Georadar system and 70 MHz, 200 MHz and 500 MHz frequency antennas. After preliminary data analysis, the 200 MHz antenna was selected as the more adequate, providing the better combination of investigation depth (3-4 m) and vertical resolution (0.1-0.2 m). The time-depth conversion on the axis perpendicular to the excavation faces was performed using a constant value of propagation velocity, evaluated from the modelling of subsurface scattering diffractions (fitting hyperbolae). The velocity values obtained by hyperbola fitting of acquired GPR data was 0.09 m/ns that is consistent with the theoretical value of electrical permittivity reported in Table 1.

Experimental data were acquired on the excavation faces with parallel profiles in horizontal and vertical directions, aiming to cover the entire surface of the faces. A similar scheme was used for all the acquisitions, with 6-8 horizontal and 3 vertical profiles, depending on logistical issues. Figure 3b shows an example acquisition scheme, with the resulting data oriented with respect to the excavation drill. For the acquisitions, appropriate elevation machinery (see Figures 9a and 12a) have been used to reach the top of the excavation face and move laterally within it.

Acquired data were processed with Reflexw5.0 (Windows OS) software using the most suitable processing flow to maximise the signal/noise ratio and to emphasize the information content. The processing flow for all the radargrams reported in the following was composed of: two static corrections (move start-time: to eliminate the first 10 ns, correspondent to the passing of the radar pulse in the air before reaching the rock, and time cut: to limit the investigated range to 100 ns), a dewowing filter with time window of 10 ns, two gain operations (a compensation for geometrical divergence with scaling factor of 0.4 and a gain function, defined as $g(t) = (1 + \frac{0.2}{pulse\ width} t)e^{(\frac{0.02}{8.69}t)}$) and a removal of the background noise (based on the average of all the traces).

1 In order to visualize the spatial distribution of the anomalies behind the excavation faces, the single
 2 radar profiles were combined to build a three-dimensional volume with Voxler software. Horizontal
 3 and vertical radargrams were juxtaposed as shown in Figure 3b and elaborated to create a 3D
 4 reconstruction of the anomalies. For this aim, an appropriate colour scale representing absolute radar
 5 amplitudes (Figure 3b) was adopted for all the presented Figures. Anomalies were identified based
 6 on appropriate thresholds on this colour scale. The value of imposed thresholds varies depending on
 7 the permittivity contrast between the gypsum and the anomaly and on the depth of the anomaly itself.



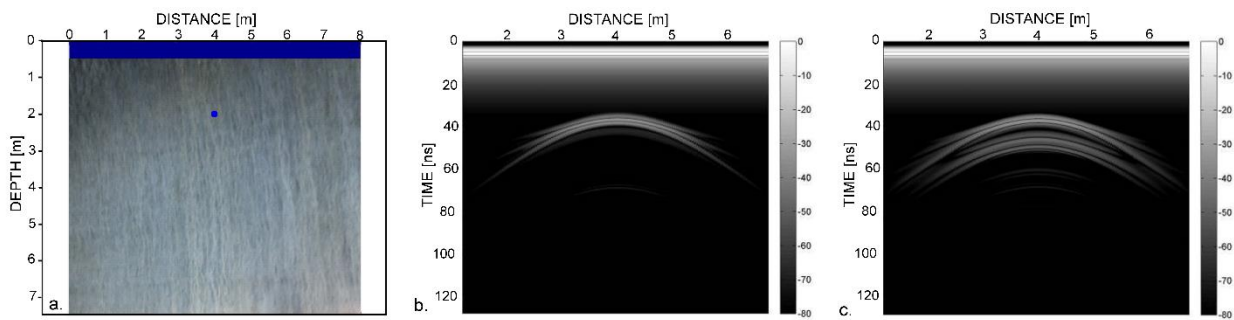
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 9 *Figure 3 a. Geometrical orientation of the numerical models with respect to the quarry face and a generic simulated anomaly. b.*
 10 *General radar acquisition scheme on the quarry faces.*

11 4 Modeling results

12 4.1 Conduits

13 The presence in the orebody of karst conduits was simulated with a circular anomaly with diameter
 14 of 20 cm in a homogeneous volume of gypsum (Fig. 4a). Synthetic radargrams in case of empty
 15 conduit (Fig. 4b) and water-filled conduit (Fig. 4c) were simulated. Results show, in both the

1 simulations, a hyperbolic signal with apex coincident with the position of the circular anomaly. In the
 2 case of water-filled conduit, multiple hyperbolae are recognizable under the principal one. The
 3 presence of water indeed triggers a ringing phenomenon and multiple hyperbola are created when the
 4 radar-wave passes through the fluid (Fig. 4c). On the contrary, when the conduit is empty, the high
 5 radar-wave propagation velocity in air brings to an overlap of the multiple hyperbola (fig. 4b).
 6 Different models with increasing depth of the anomaly where also produced, confirming the anomaly
 7 visibility till a maximum investigation depth of 5 m.

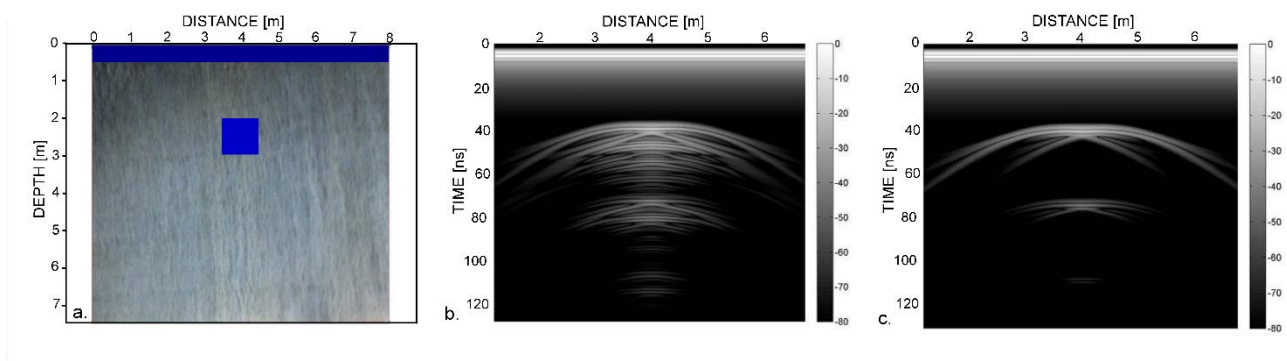


8
 9 *Figure 4 a. Reference model with a cylindrical anomaly with diameter of 20 cm at a depth of 1.5 m in an uniform volume of gypsum;*
 10 *b. Synthetic radargram with the anomaly considered as void; c. Synthetic radargram with the anomaly considered as filled of water.*

11 4.2 Cavities

12 Figure 5a shows a model simulating the presence of a karst cavity with regular shape and size of 1m
 13 x 1m. Results refer to the absence of filling and to the presence of water within the anomaly
 14 (respectively, Figure 5b and 5c). In both simulated radargrams, the interference of several hyperbolic
 15 signals producing a big and complex anomaly is evidenced. The absence of filling brings to a further
 16 multiplication of signal reflections (ringing) within the void cavity (Fig. 5b). These reflections are
 17 strongly attenuated in the water-filled cavity (Fig. 5c), where the signal is less complex and more
 18 defined. In this last condition, main reflections of the top and the bottom of the cavity are possible to
 19 be recognized. The presence of water seems therefore to generate opposite effects in the simulations
 20 of small conduits and big cavities. In the first case, an increased ringing due to the anomaly is
 21 recognized (Fig. 4c), while in the second case the ringing is strongly reduced (Fig. 5c). This apparent

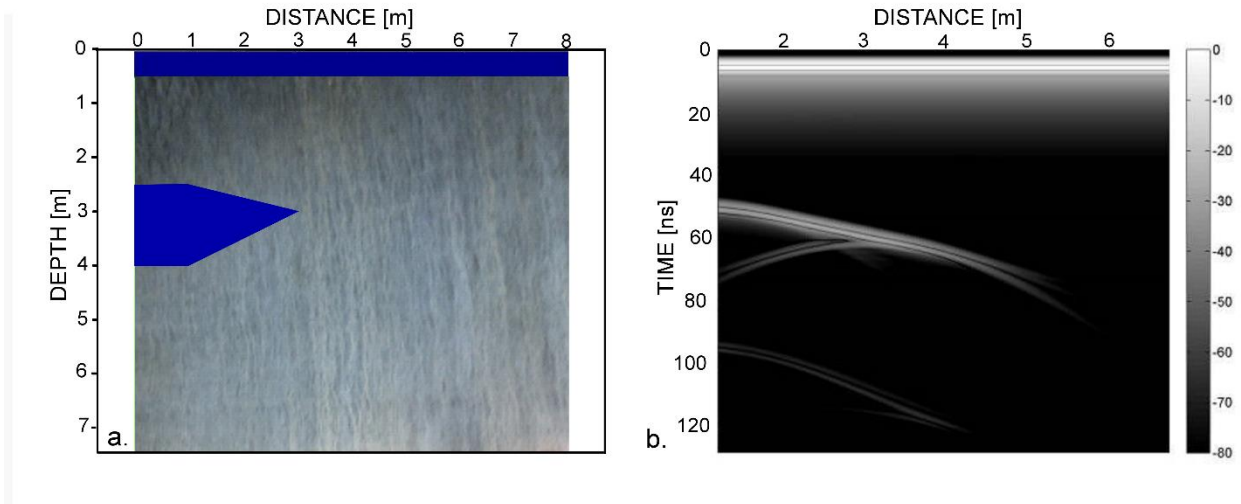
1 inconsistency can be explained considering the size of the anomalies compared to the radar velocity
2 in water or air: in small dimensions anomalies (conduits) the velocity reduction due to water makes
3 the arrival times of multiple reflections at the anomaly borders shortly delayed and partially
4 superimposed in the acquisition time; in anomalies with greater dimensions (cavities) the arrival times
5 are instead strongly delayed and do not superimpose in the acquisition time. The opposite is true for
6 the air filled anomalies. These considerations are related to the fact that the arrival times of different
7 reflection events is related both to the space travelled (anomaly dimensions) and to the velocity of
8 propagation within this space (filling material).



9
10 *Figure 5 a. Reference model with a square anomaly with sizes of 1m x 1m at a depth of 1.5 m in an uniform volume of gypsum; b.*
11 *Synthetic radargram with the anomaly considered as void; c. Synthetic radargram with the anomaly considered as filled of water.*

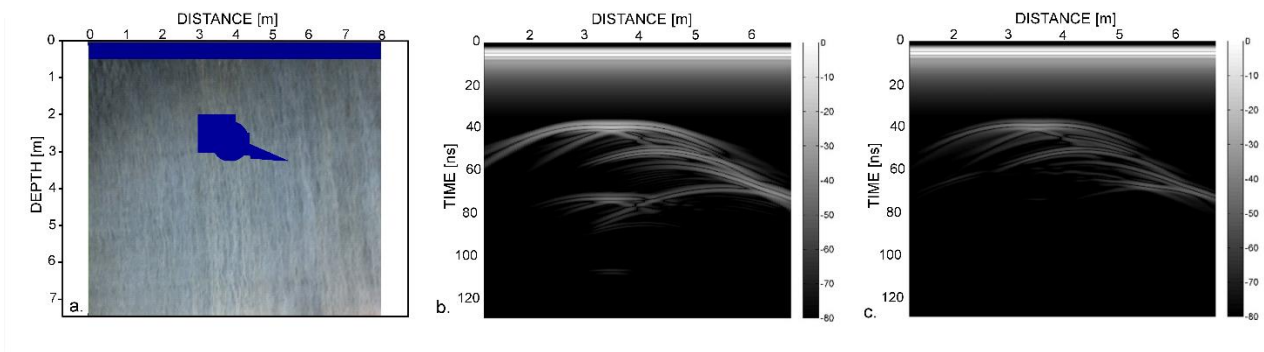
12 The framework of a natural rock mass may present complex situations where the schematization of a
13 square cavity with regular shape is insufficient to correctly interpret the GPR outputs. Differences in
14 position, sizes and shape of the cavity can significantly influence the GPR results. With this aim
15 different cavity shapes and position were further simulated (also in comparison with the following
16 acquired experimental data). Figure 6 shows an example of a different cavity shape and location. The
17 cavity modelled in Figure 6a, located at the left of the investigated face, with a sharp tip towards the
18 centre of the section, gives an output considerably different from the idealized square cavity in Figure

1 5. Still this water filled cavity is clearly recognized and approximate cavity dimensions can be
2 deduced from the radargram considering top and bottom reflections.



3
4 *Figure 6 a. Reference model with carst cave with irregular shape at a depth of 2 m in an uniform volume of gypsum; b. Synthetic*
5 *radargram with the anomaly considered as filled by water.*

6 Another potential complex situation is due to the interference of a cavity with lateral conduits,
7 possibly responsible of the alimentation and the connection with the karst system. Fig. 7a presents a
8 schematic model of this situation.



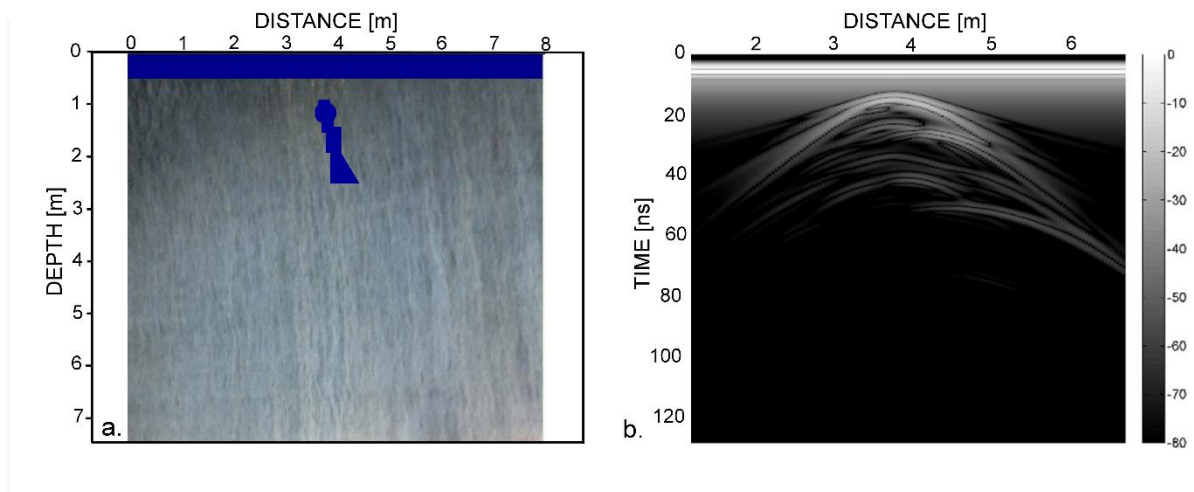
9
10 *Figure 7 a. Reference model with carst cave connected with a conduit at a depth of 1.5 m in an uniform volume of gypsum; b. Synthetic*
11 *radargram with the anomaly considered as filled of water; c. Synthetic radargram with the anomaly considered as filled of clay*

12 The cavity with its conduit were considered as filled by water (Fig. 7b) or filled by clay (Fig. 7c) in
13 the simulations. Results show a large hyperbolic signal, similar to Figure 5b, for the main cavity but

1 interfering with several closer hyperbolic signals in the right, where the conduit is located. The
2 presence of clay within the cavity with respect to the water further slows down the radar velocity and
3 increases the attenuation so that the reflection from the cavity bottom is no more visible in the
4 simulated radargrams.

5 4.3 Fractures

6 The presence of a shallow open water-bearing fracture oriented almost perpendicular to the
7 excavation face was simulated as shown in Figure 8a. Simulated fracture aperture was of about the
8 same order of small conduits (i.e. 20 cm). The synthetic radargram shows one principal hyperbole
9 intensified and complicated by the overlap with several hyperbolic signals in the right, where the
10 fracture is oriented.



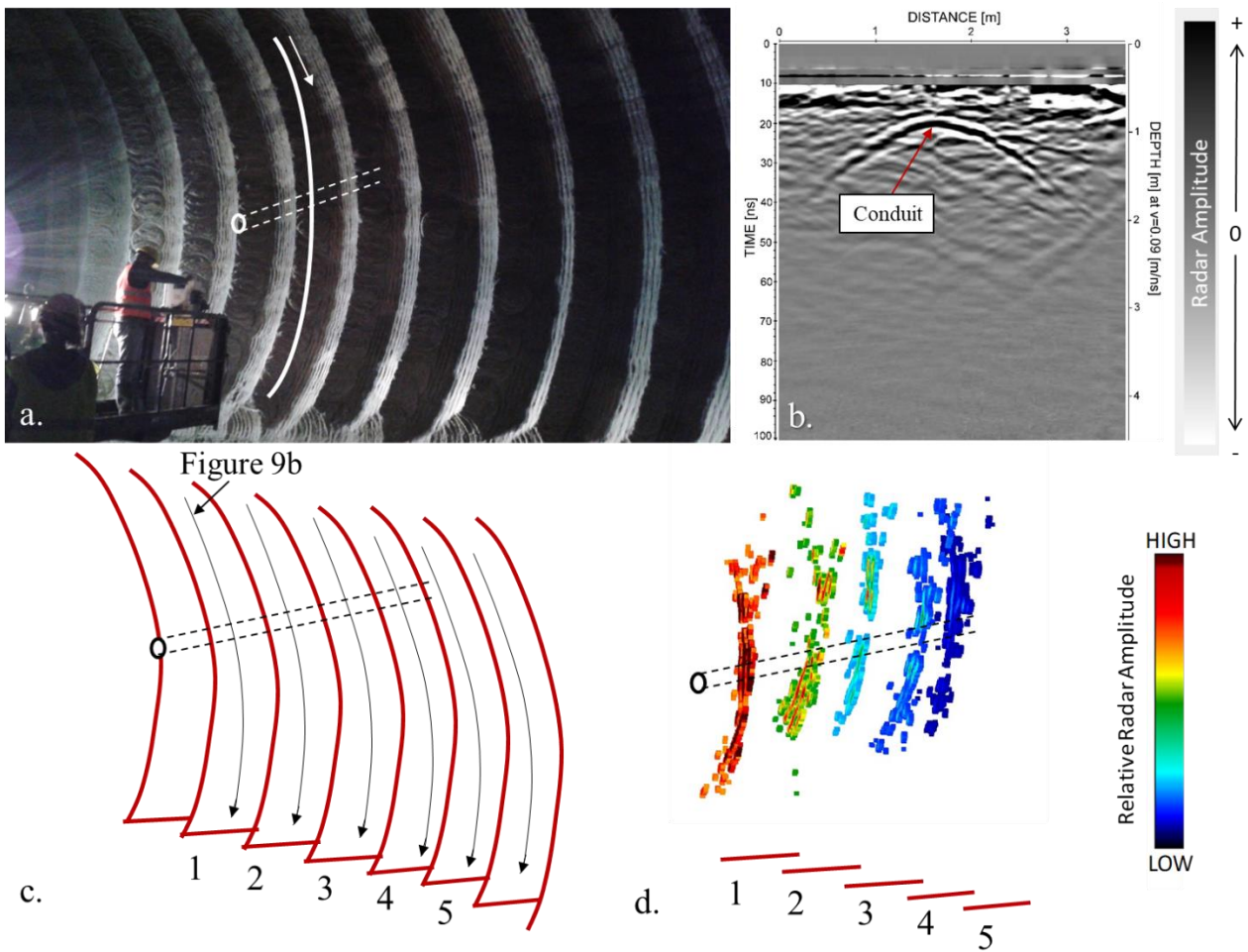
11
12 *Figure 8 a. Reference model to simulate the presence of an open fracture almost perpendicular to the excavation surface; b Simulated*
13 *synthetic radargram with the anomaly considered as filled of water*

14 5 Survey results

16 5.1 Conduits

17 An air filled drilled hole (10 cm diameter) was used to simulate a small karst conduit. As shown in
18 Figure 9a, c and d, the hole is oriented almost perpendicular to the lateral wall of the drift, entering

1 the gypsum ore body on the side of the excavated gallery. Six vertical radar profiles at increasing
 2 distances from the hole were acquired along the “waved” wall, on the “wave-face” parallel to the
 3 drilled hole direction. The radar input is therefore directed toward the hole but the hole itself will
 4 result at increasing distances (from 1 to 6 “waves”) from the antenna. Radar output for the shallower
 5 distance profile (Fig. 9b) gives a well-defined hyperbole, without multiple reflections, concordant
 6 with the model for a void conduit in Figure 4b.



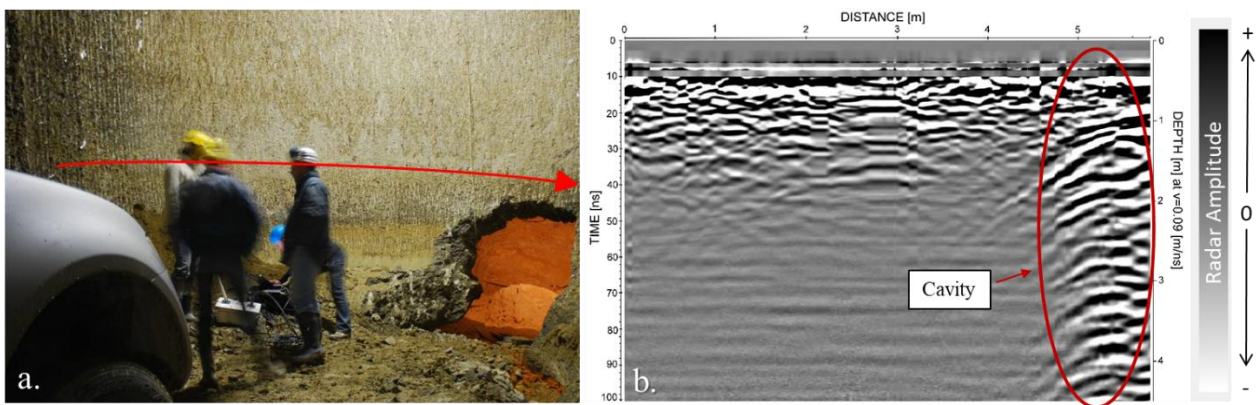
7
 8 *Figure 9 a. Radar acquisition of a drilled hole; b. Radar output with hole depth of 0.5 m; c. Acquisition scheme of the six profiles; d.*
 9 *Three-dimensional reconstruction*

10 With the increasing distance from the hole, the signal results more attenuated, being completely
 11 obliterated from environmental noise in the sixth profile (distance from the hole of 2.5 m). This
 12 suggests a threshold for the investigation depth of the method (Caselle et al. 2016). This threshold is

1 significantly lower than the one evidenced with numerical simulations, given the added background
2 noise. The hyperbola apexes from the different profiles are aligned and their depth coherently
3 increases. Since the processing flow was uniform for all the profiles, the hyperbolic signal has
4 decreasing amplitude with the increase of the depth. Therefore, in the three-dimensional
5 reconstruction in Figure 9d, decreasing values of threshold amplitude were imposed to the GPR
6 profiles with increasing distance from the target. Still, results from this visualization allow for a
7 correct evaluation of the elongation direction and spatial position of the hole. These results suggest
8 that the identification of small karst conduits with different parallel profiles is possible.

9 5.2 Cavities

10 A GPR profile was acquired on the excavation face in front of the karst room cropped out after the
11 2005 inrush in Moncalvo quarry (Fig. 10a). The radar output (Fig. 10b) shows, in the right, a marked,
12 multiple ringing signal referable to the cavity. The absence of filling bring to create, as in the model
13 in Figure 5b, a complex output due to the multiple reflections (ringing) of the signal within the void
14 cavity.

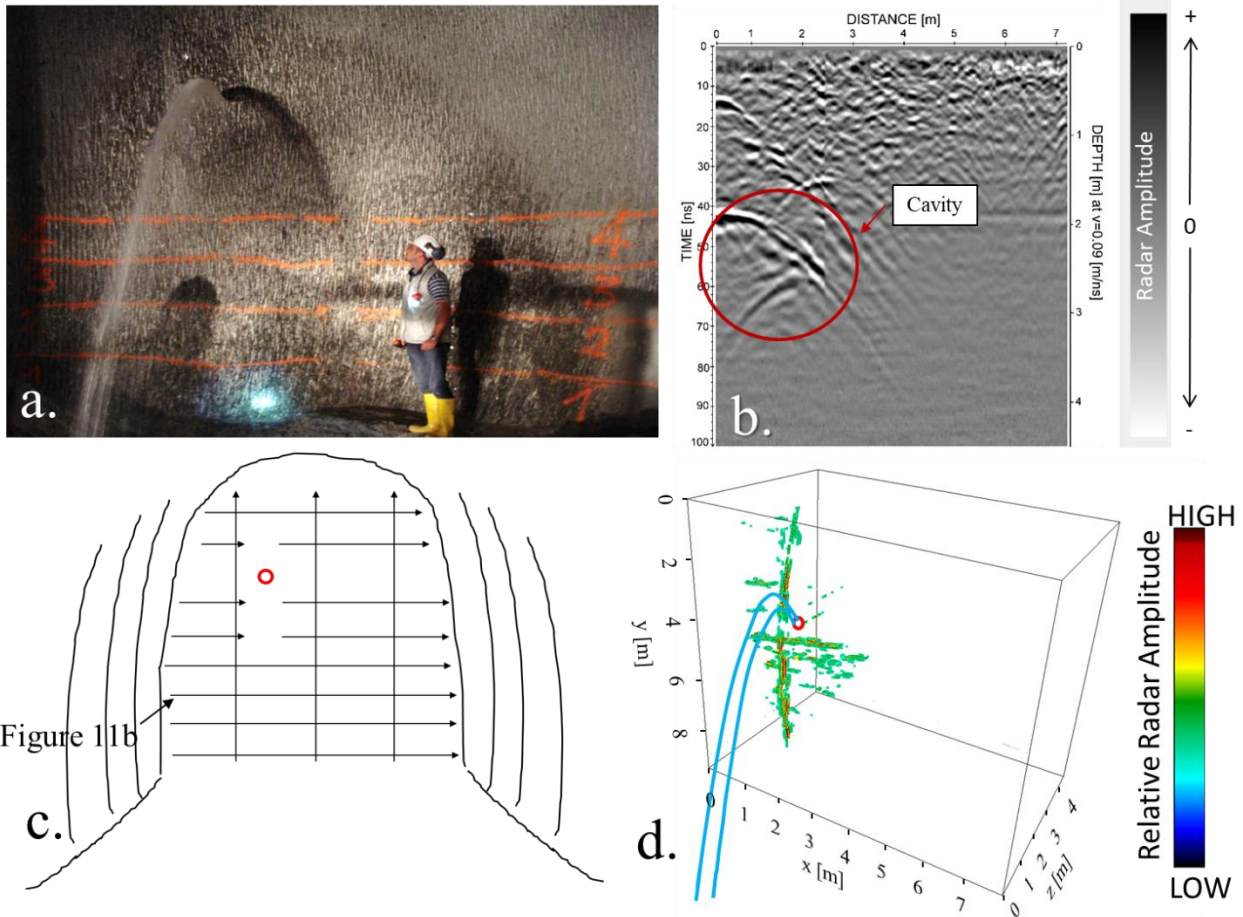


15
16 *Figure 10 a. Excavation face in front of the karst room cropped out after the 2005 inrush; b. Radar output*

17 Two quarry faces were also selected (one from Moncalvo quarry and one from Calliano quarry) to
18 test the detectability of cavities filled by water. In the tested faces, the excavations have been
19 interrupted because the drilling of horizontal boreholes highlighted the presence of water, that, as

1 shown in Figures 11a and 12a, was actually stilling from the holes when the present study was
2 performed. Surveys were therefore devoted to the potential identification of the water cavities or karst
3 conduits alimenting these stillings.

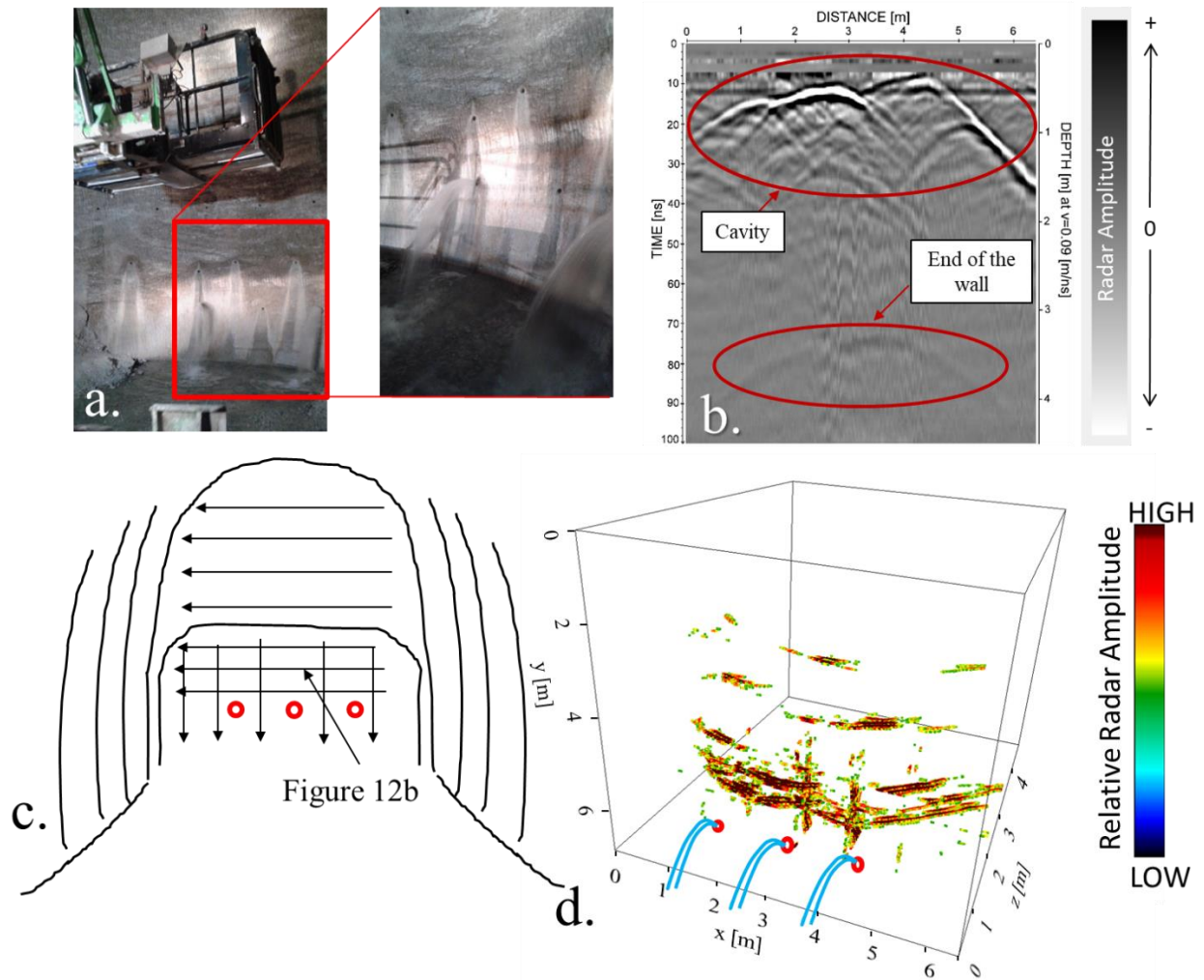
4 Figure 11 refers to the GPR data acquired in the Moncalvo quarry. Fresh pressurized water flows
5 through the vent in the high-left portion of the excavation face (Fig.11a). Radar acquisition was
6 performed following the scheme in Figure 11c. An example horizontal GPR profile shows, in the left,
7 a complex signal due to the interference of two hyperbolae at different depths and x-position (Fig.
8 11b). The radar anomaly is significantly similar to the one simulated in Figure 6, suggesting a
9 geometrically similar situation. Three-dimensional reconstruction (Fig. 11d) shows the good
10 alignment of the hyperbolic signals from horizontal and vertical profiles, with concordant position
11 and depth. From these multiple profiles alignments, the estimation of the approximate location and
12 dimensions of the water filled void is therefore possible.



1

2 *Figure 11 a. Excavation front in Moncalvo quarry with water leakage.; b. Radar output from an horizontal profile; c. Acquisition*
 3 *scheme used for radar profiles; d. Three-dimensional reconstruction.*

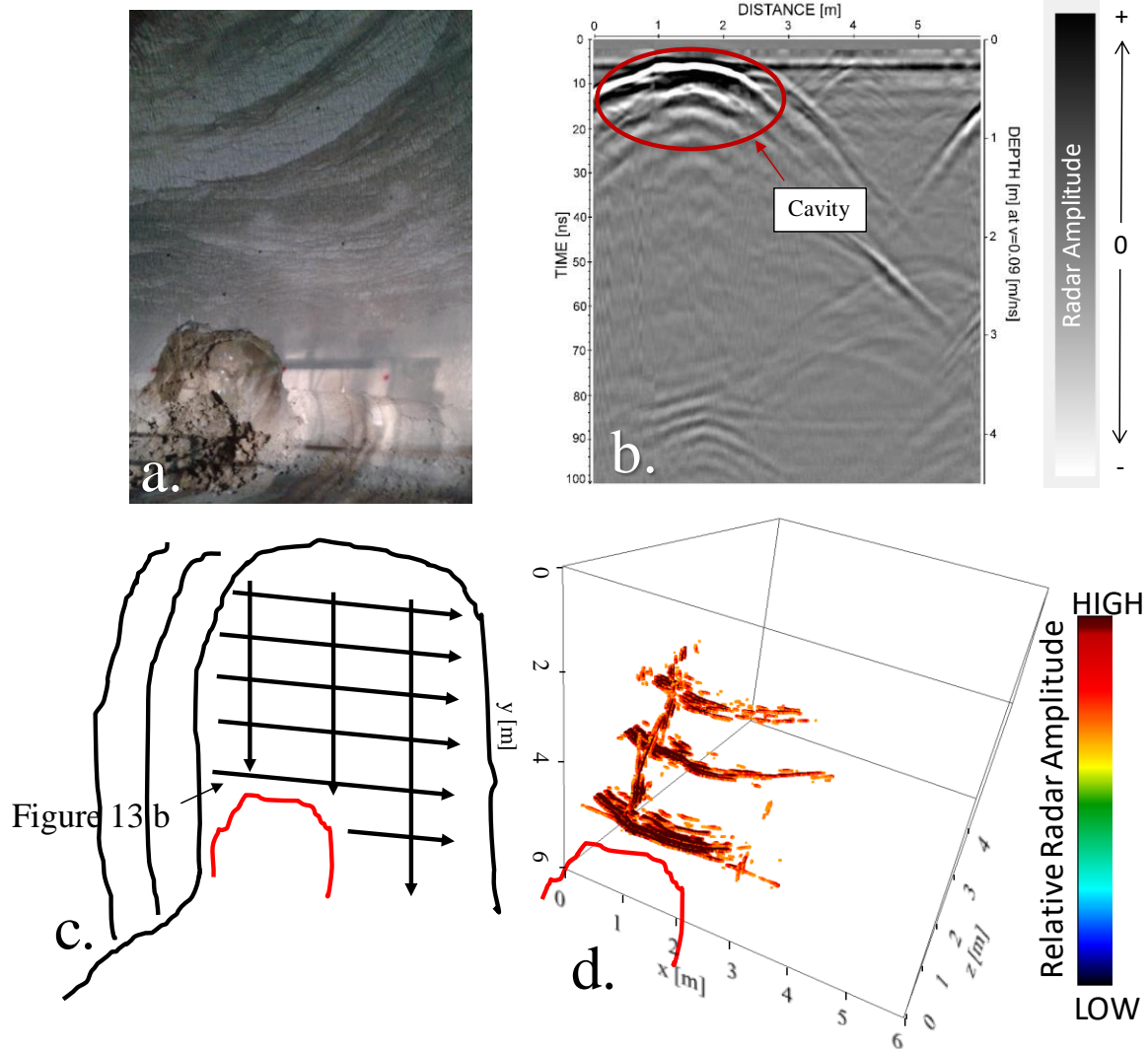
4 Figure 12 refers to the water leakage in the underground Calliano quarry. When this study was
 5 performed, water was flowing through three holes in the lower part of the excavation face. GPR
 6 profiles were acquired following the acquisition scheme in Fig. 12c. Output of the second horizontal
 7 profile from the bottom shows a well-defined anomaly due to the interference of 3 hyperbolae with
 8 apexes at 1, 2.5 and 3.5 m from the profile start (Fig. 12b). A strong signal at 75ns (about 3.5 m) can
 9 be attributed to the end of the investigated wall (which has a thickness of about 3-4 m). Similar
 10 evidences may be recognized in all the horizontal profiles. Vertical profiles show continuous
 11 horizontal reflectors for their entire height. Figure 12d shows the 3d volume reconstruction. Signals
 12 from vertical and horizontal profiles delineate a large area in the bottom of the excavation front
 13 potentially interested by the water-filled cavity.



1

2 *Figure 12 a. Excavation front with water leakage in Calliano quarry; b. Radar output from an horizontal profile; c. Acquisition scheme*
 3 *used for radar profiles; d. Three-dimensional reconstruction.*

4 Figure 13 describes the radar investigation of a potential clay-filled cavity in the Calliano quarry. A
 5 compact clay body was observed through an opening in the low-left part of the drift face (Fig. 13a).
 6 Radar analyses were performed following the investigation scheme in Figure 13c. GPR outputs show
 7 the presence of well-defined hyperbolic anomalies in the horizontal profiles (e.g. the lower complete
 8 horizontal profile in Fig. 13b). The vertical profile above the opening contains a clear reflector
 9 dipping towards the opening in the low part of the wall. The resulting 3d reconstruction (Fig. 13d),
 10 synthesizing the information from horizontal and vertical profiles, shows the good agreement of the
 11 signals in the single profiles, concordant to describe the presence of an inclined anomalous body.



1

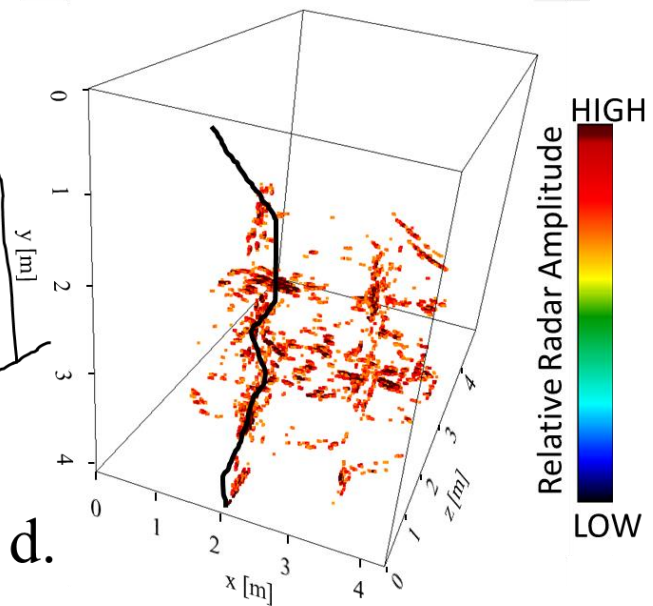
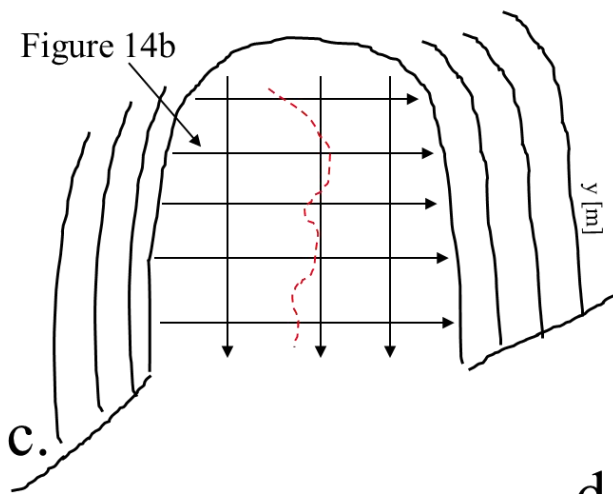
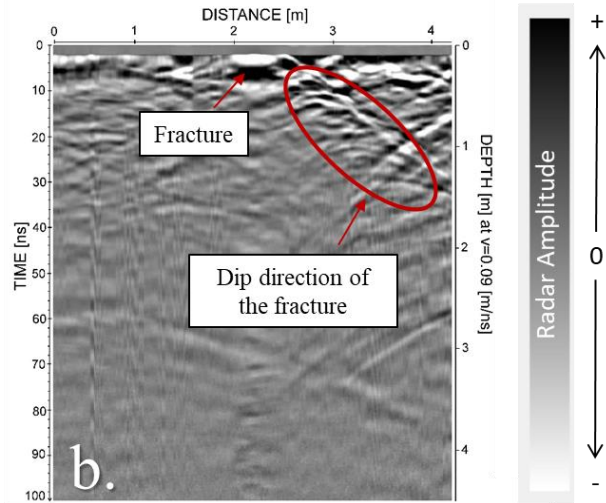
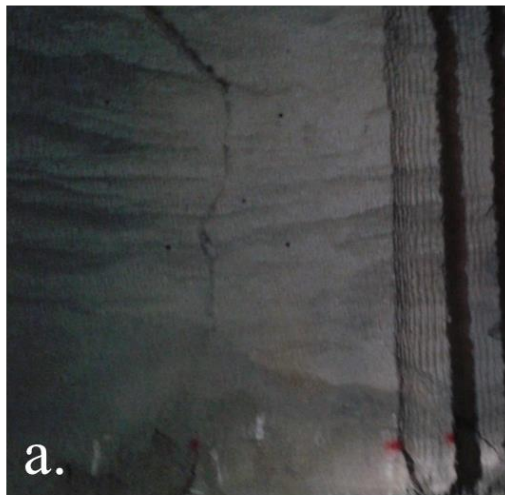
2 *Figure 13 a. Excavation face with outcropping of a clay body; b. Radar output from an horizontal profile; c. Acquisition scheme used*
 3 *for radar profiles; d. Three-dimensional reconstruction*

4

5.3 Fractures

5

An open sub-vertical fracture was recognized and analysed in the Calliano quarry (Figure 14a). The analysis with GPR, performed with vertical and horizontal profiles following the scheme in Figure 14c, shows an acceptable detectability of the structure. Horizontal profiles (e.g. Fig. 14b) report local hyperbolic anomalies, moving to the left on the top of the face, reproducing the orientation of the fracture. An intensification of the signal in the right branch of the hyperbole suggests an orientation of the structure in that direction, in agreement with the synthetic radargram in Figure 8b.



1

2 *Figure 14 a. Excavation front with the open sub-vertical fracture; b. Radar output from an horizontal profile; c. Acquisition scheme*
 3 *used for radar profiles; d. Three-dimensional reconstruction.*

4 With respect to numerical simulations, reduced ringing effect was evidenced in the acquired data,
 5 suggesting the presence of an open fracture with air filling. This is corroborated by the absence of
 6 water inflows at the excavation face. The additional reflection in the right part of the radargram at
 7 about 80 ns (Fig. 14b) is probably due to the radar reflection on the lateral wall of the analysed face.
 8 Vertical profiles, subparallel to the fracture outcrop, contain vertical signals, oriented parallel to the
 9 face. The 3d reconstruction (Figure 14d) shows concentrations of anomalies in correspondence of the
 10 fracture cropping and in the right part of the volume. This last part can be related to the reflection of

1 the signal on the lateral wall for increased times, but also to a potential parallel fracture with the one
2 evidenced in the front.

3 6 Discussions and Conclusions

4 The principal elements of karst hazard (conduits, cavities and fractures) in gypsum orebodies were
5 investigated and analyzed with Ground Penetrating Radar (GPR) techniques. Electromagnetic models
6 were produced for each anomaly, considering the influence of different possible fillings (air, water
7 and clay). The geological complexity was considered in the modeling of karst caves to obtain more
8 realistic frameworks. Models show clear outputs for all the considered situations. The discrimination
9 between empty and water-filled anomalies was possible thanks to the different propagation velocities
10 and absorption power. Particularly, small karst conduits, or fractures, filled with water are evidenced
11 by the presence of localized hyperbolic signals and increased ringing effects with respect to the same
12 anomalies filled with air. Cavities are instead evidenced by more complicated reflection patterns,
13 related to their shapes and dimensions; the ringing effect is promoted in presence of air with respect
14 to water or clay fillings.

15 A wide GPR survey campaign was performed in two underground gypsum quarries with evidences
16 of karst phenomenon. Targets ahead the excavation faces were investigated through horizontal and
17 vertical GPR profiles. Output radargrams were processed and described. Three-dimensional
18 reconstructions were proposed, aiming to create an easily understandable and complete visualisation
19 of the GPR outputs.

20 From a comparison of both numerical simulations and field surveys, it was possible to evaluate the
21 potentiality of GPR for the present case study, in particular:

- 22 - Karst conduits: a successful identification of karst conduits with diameter above 10 cm was
23 verified up to a depth of about 2 m. The radar output is a single hyperbolic signal with apex
24 coincident with the position of the circular anomaly. Potential discrimination with respect to

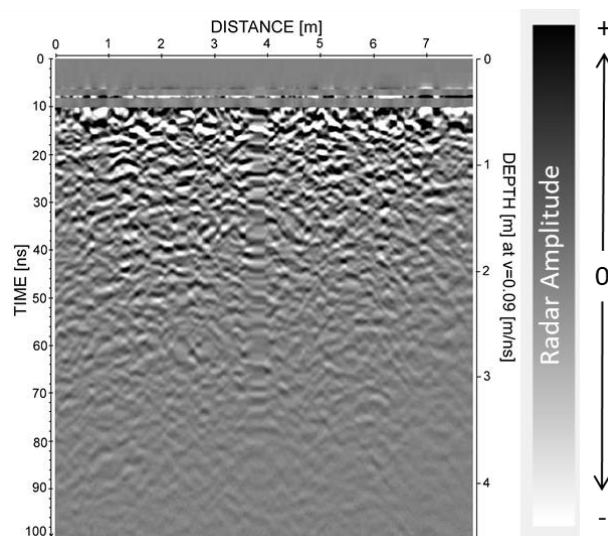
1 the water filling of these conduits are also evidenced. These last discriminations are related to
2 the presence or not of multiple hyperbolic reflections for the same spatial location. In case of
3 water within the conduits, the ringing phenomenon due to the slowing of the radar signal is
4 indeed promoted (see Figures 4c and 7b) with respect to the presence of air within the conduit
5 (see Figures 4b and 9b);

- 6 - Karst cavities: a successful identification of karst cavities has been obtained in all the
7 simulated and real acquisitions. The radar output consists of a large and very intense anomaly,
8 resulting by the interference of several hyperbolic signals. Cavities with irregular shapes may
9 complicate the radar anomalies, creating big and complex signals. Contrary to the results
10 obtained over karst conduits, air filled cavities are depicted with increasing ringing
11 phenomenon (see Figures 5b and 10b) with respect to clay or water filled cavities (see Figures
12 5c, 11b and 12b). This last effect can be related to the increased attenuation of the radar signal
13 in presence of clay or water which does not allow multiple reflections within the same cavity.
14 In the case of water or clay filling, the bottom of the cavity is also not always possible to be
15 discriminated, depending on the depth of the cavity (see Figures 7b and 7c).

- 16 - Open fractures: if the fracture is oriented perpendicular (or almost perpendicular) to the
17 excavation face, the radar output can be described as a principal hyperbole intensified and
18 complicated by the overlap with several hyperbolic signals in the direction where the fracture
19 is oriented. Having similar dimensions to karst conduits, also in open fractures the water
20 filling promotes the radar wave ringing with respect to the air filling (see Fig. 8b with respect
21 to Fig. 14b). Open fractures perpendicular to the excavation face are critical to be identified
22 in terms of dipping direction.

23 For exploitation purposes, the assessment of the dangerousness of a structure and the assignment of
24 a specific warning degree to each GPR scenario is fundamental. Taking as reference the radar output
25 relative to an undisturbed quarry face (Figure 15), all the presented anomalies are detectable and a
26 first degree of warning could be assigned to all those situations. Additional discriminations can be
27 based on the size of the anomaly and, particularly, on its filling. Results of this study indicate a good

1 detectability of the size of the anomaly on the base of the lateral extension of the hyperbolic signal
2 (or the combined signal of several hyperbolae). The assessment of the approximate size of the
3 anomaly is not only important in itself for the warning purposes, but also for the discrimination of
4 the filling. Indeed, as already claimed, the water filling has different effects on the GPR output
5 depending on the size of the anomaly. The presented study offers therefore a preliminary guide to
6 predict the dangerousness of a quarry face on the base of GPR analyses.



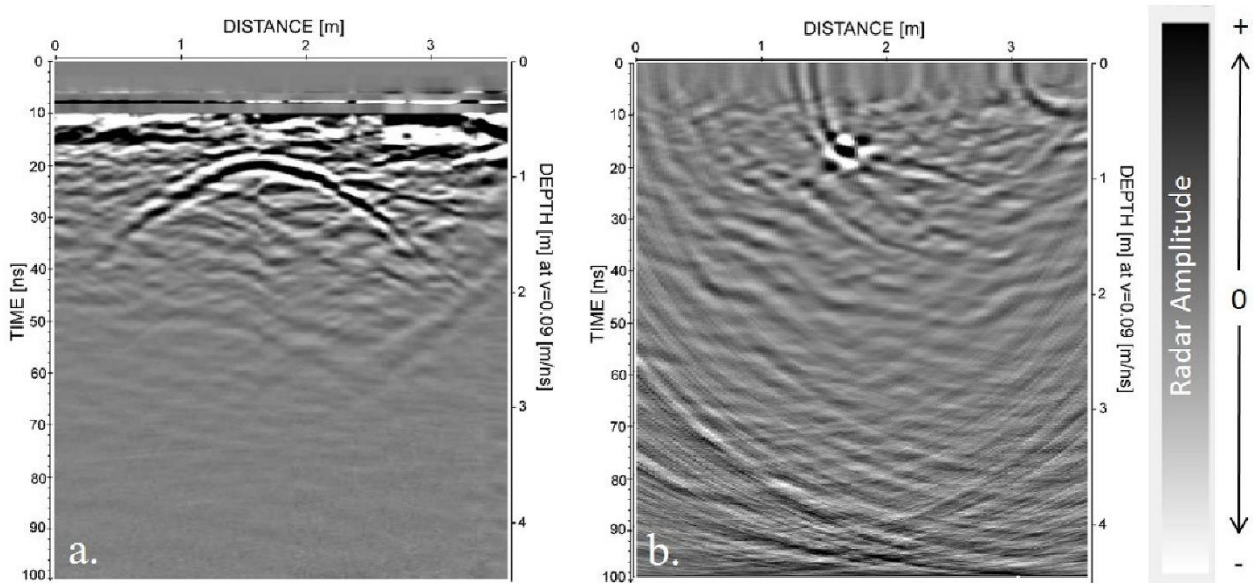
7

8 *Figure 15 Radar output in correspondence of an undisturbed, integer quarry face, without the presence of anomalies.*

9 For the low investigation depth of GPR survey method (about 3 meters within this material), a suitable
10 way to apply this technique would include the implementation of a system of continuous automatic
11 monitoring. A continuous upgrade of GPR imaging of the gypsum orebody, concomitant with the
12 excavation progress, would provide reliable previsions, with positive effects on the safety and the
13 efficiency of the exploitation. With this aim the data migration was not included in the processing
14 flow in order to maintain a fast and light data processing, in view of a possible real-time application
15 of the methodology, concomitant with the excavation progress.

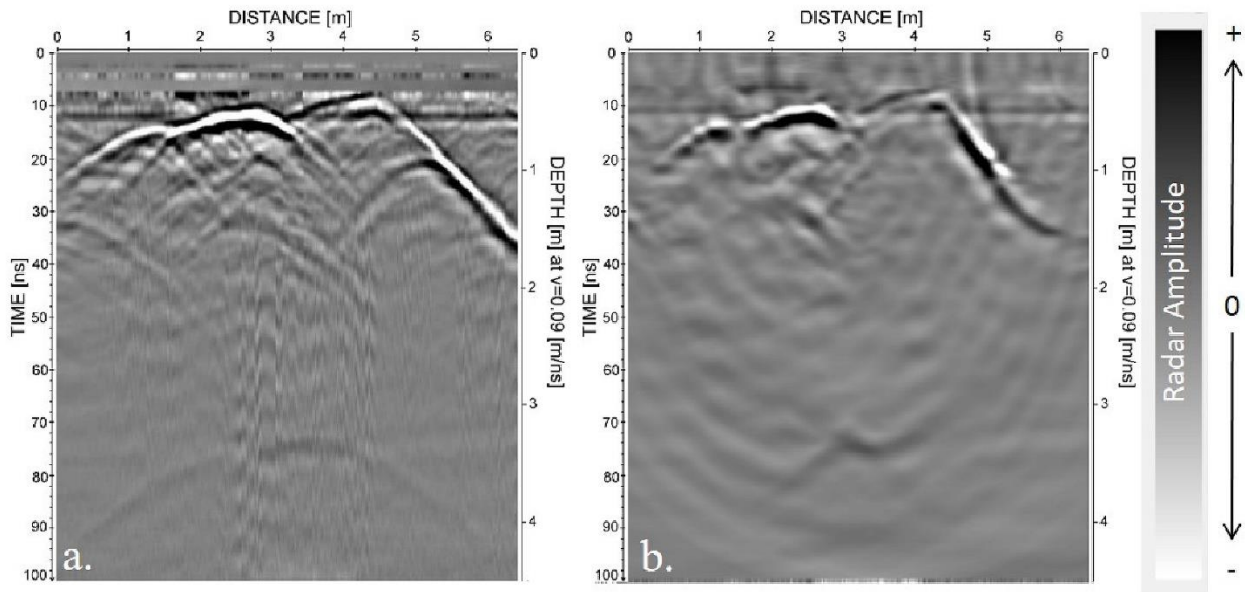
16 Two examples of application of migration process on the experimental data are shown hereafter in
17 Figures 16 and 17. As could be expected, the migration significantly affects the data visualization

1 when a single clear hyperbolic pattern is recognized (conduits example in Figure 16). In this case, the
2 hyperbole collapses in a single point better visualizing the drilled hole shape and dimensions.
3 However, the migration process only improves the imaging quality but the delectability of the conduit
4 is not particularly increased. On the contrary, the presence of a point instead of a hyperbole is more
5 difficult to be recognized at higher depths.



6
7 *Figure 16 Migration process of data referred to a karst conduit (figure 9b).*

8 Similar considerations can apply in the presence of a karst cavity (Figure 17). The migrated image
9 better allows to define the real cavity shape by collapsing multiple reflection patterns on its
10 boundaries.



1

2 *Figure 17 Migration process on data referred to a karst cavity (figure 12b).*

3 Nevertheless, again, if the survey results have to be used for preliminary warning purposes, even
 4 under the eyes of non GPR expert users, the non migrated radargrams contain more signal and
 5 information that can allow for the recognition of an anomaly in the gypsum formation. Based on this,
 6 a clear warning can be established. After this warning, shape and filling discriminations could be
 7 performed by more sophisticated processing (including migration) and by comparison with synthetic
 8 simulations reported in this paper.

9

10

11

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