

AperTO - Archivio Istituzionale Open Access dell'Università di Torino

## In silico tensile tests and design of hierarchical graphene fibres and composites

### **This is the author's manuscript**

*Original Citation:*

*Availability:*

This version is available <http://hdl.handle.net/2318/136489> since 2016-06-28T13:38:59Z

*Published version:*

DOI:10.1002/pssb.201200977

*Terms of use:*

Open Access

Anyone can freely access the full text of works made available as "Open Access". Works made available under a Creative Commons license can be used according to the terms and conditions of said license. Use of all other works requires consent of the right holder (author or publisher) if not exempted from copyright protection by the applicable law.

(Article begins on next page)

1  
2  
3  
4  
5  
6  
7  
8  
9  
10  
11  
12  
13  
14  
15  
16  
17  
18  
19  
20  
21  
22  
23  
24  
25  
26  
27  
28  
29  
30  
31  
32  
33  
34  
35  
36  
37  
38  
39  
40  
41  
42  
43  
44  
45  
46  
47  
48  
49  
50  
51  
52  
53  
54  
55  
56  
57



# UNIVERSITÀ DEGLI STUDI DI TORINO

*This is an author version of the contribution published on:*

*[Physica Status Solidi (b), Volume 250, Issue 8, pages 1492–1495, August 2013,*

*DOI: 10.1002/pssb.201200977]*

*The final version is available at:*

*<http://onlinelibrary.wiley.com/doi/10.1002/pssb.201200977/abstract>*

# In silico tensile tests of graphene fibres

Federico Bosia <sup>\*,1</sup> and Nicola M. Pugno <sup>\*\*,2</sup>

<sup>1</sup> Department of Physics and “Nanostructured Interfaces and Surfaces” Centre of Excellence, University of Torino, Via P.Giuria 1, 10125, Italy

<sup>2</sup> Department of Civil, Environmental and Mechanical Engineering, University of Trento, via Mesiano 77, 38123 Trento, Italy

**Keywords** Graphene, mechanical properties, simulations, hierarchy

\* Corresponding author: federico.bosia@unito.it, Phone: +39 011 6707889, Fax: +39 011 6707020

\*\* nicola.pugno@unitn.it, Phone: +39 +39 338 6275625, Fax: +39 0461 282599

**Abstract.** In this contribution, we apply a hierarchical fibre bundle model, previously developed to estimate the mechanical properties of multiscale carbon nanotube-based structures, to the case of graphene macroscopic cables. The nonlinear elastic properties of graphene and its exceptional intrinsic strength, with mean Young’s modulus of 1 TPa, third-order elastic stiffness of  $-2.0$  TPa, and intrinsic strength of 130 GPa, are drawn from recent experimental studies. The model allows to derive macroscopic characteristics like strength, stiffness, toughness

as a function of hierarchical structure, starting from statistically distributed properties at the nanoscale, and without the introduction of additional ad hoc parameters. The influence of the presence of defects in the graphene bundles is evaluated. We also analyze the properties of graphene-reinforced composites, including the influence of the volume fraction of a ductile polymeric matrix. We show that the composite properties can be engineered to optimize strength and/or stiffness, and that the present model can be a useful tool to help pursue this objective

**1 Introduction** In recent years, much effort has gone into investigating Graphene for its exceptional electronic, thermal, optical and mechanical properties. Various different graphene nano/micro-structures have by now been synthesized and characterized, including graphene paper [2], graphene nanoribbons [3], and also macroscopic assembled graphene fibres [4]. In addition, large area growth techniques have been increasingly developed thanks to specific research in this direction [5,6]. Another important field is that of graphene-based composites, which could provide the means to harness graphene’s exceptional properties for applications [7].

From a mechanical point of view, graphene can be considered “the strongest material ever measured”, ever since Lee and co-workers managed to measure the elastic properties and intrinsic breaking strength of free-standing monolayer graphene membranes by nanoindentation in an atomic force microscope [1]. In this study, graphene was found to display a nonlinear elastic behaviour of the type

$$\sigma = E\varepsilon + D\varepsilon^2 \quad (1)$$

where  $\sigma$  is stress,  $\varepsilon$  is strain,  $E = (1.0 \pm 0.1)$  TPa and  $D = (-2.0 \pm 0.4)$  TPa. Moreover, its measured intrinsic strength was  $\sigma_f = (130 \pm 10)$  GPa, which is the highest value found for any material in nature. However, it is unclear what the effect of defects, grain boundaries etc. could have

on these values. In carbon nanotubes (CNT), a low-dimensional material like graphene, the introduction of a single defect can determine a drop of Young’s modulus of up to 20% [8]. Another question is: in graphene composites, how can we optimize mechanical performance (stiffness, strength, toughness...) by varying constituent material properties, mixing ratio, hierarchical structure, or other parameters? Clearly, experimental investigations to reply to these questions would entail very cumbersome studies, therefore it is convenient to develop numerical models to predict mechanical multiscale behaviour of graphene structures and composites. To do this, we have adopted a very simple modelling approach, previously used to perform multiscale simulations on the stiffness and strength of defective nanotube-based mega-structures [9], or for the design of supertough nanofibers inspired by spider silk [10], where CNT-polyvinyl alcohol (PVA) composites were analysed. The model is presented in Section 2 and simulation results on graphene ribbons and composites are presented in Section 3.

## 2 Hierarchical Fibre Bundle Model (HFBM)

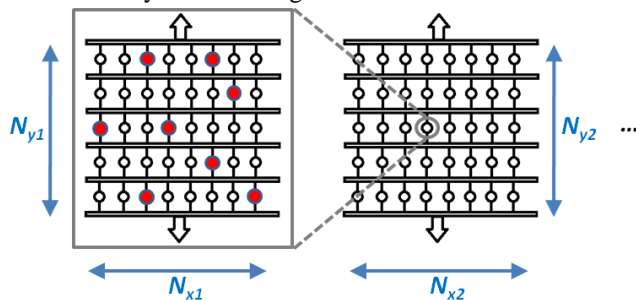
The model used here is related to that proposed by the authors in the past [9, 11], which is based on a Fibre Bundle Model (FBM) approach, and whereby a specimen is discretized in an array of springs (or “fibres”) arranged in se-

ries and parallel. The individual fibres have randomly-assigned statistically-distributed strengths, in this case according to the 2 parameter Weibull distribution, which is described by the following equation [12]:

$$p(\sigma) = \frac{m}{\sigma_0} \left( \frac{\sigma}{\sigma_0} \right)^{m-1} e^{-\left(\frac{\sigma}{\sigma_0}\right)^m} \quad (2)$$

where  $\sigma_0$  and  $m$  are the scale and shape parameters, respectively. In order to model heterogeneous media, such as in composites, the fibres of each bundle can assume different mechanical properties. The  $k$ -th fibre type is characterized by a Young's modulus  $E_k$ , length  $l_k$ , cross-sectional area  $A_k$ , and Weibull-distributed fracture strengths, the latter characterized by a scale parameter  $\sigma_{0k}$  and shape parameter  $m_k$ . The various types of fibres combine in forming "bundles", with complex mechanical behaviour emerging from the mechanical properties and arrangement of the constituent fibres. The specimen's stress-strain behaviour is determined by imposing an increasing displacement and "rupturing" individual fibres in the bundle (i.e. setting their stiffness to zero) when their statistically assigned strength is exceeded. After each fracture event, the load is redistributed uniformly among the fibres in the same bundle as the fractured one (equal load sharing). The bundle strength is obtained as the maximum stress value reached in the simulation before failure, i.e. when all parallel fibres of the bundle have failed. Since the fibre strengths are assigned randomly according to the Weibull distribution, results differ for each simulation, and average trends can be derived from repeated simulations.

The model is replicated in a hierarchical scheme at various length scales ("levels") to predict the multiscale mechanical behaviour. This is implemented as described in [9], i.e. the input mechanical behaviour of a level  $i=h-1$  "fibre" or subvolume is statistically inferred from the average output deriving from repeated level  $h$  simulations, that of a level  $i=h-2$  subvolume from level  $i=h-1$  simulations, and so on, down to the lowest hierarchical level  $i=1$ . Overall, the specimen is modelled as an ensemble of  $N_1$  subvolumes arranged in a bundle. Each of these subvolumes is in turn constituted by  $N_2$  subvolumes, arranged in a bundle as before. This scheme is applied for  $h$  "generations", up to a level  $h$  subvolume, which is constituted  $N_a$  type "a" fibres,  $N_b$  type "b" fibres, and so on. This is schematically shown in Fig.1

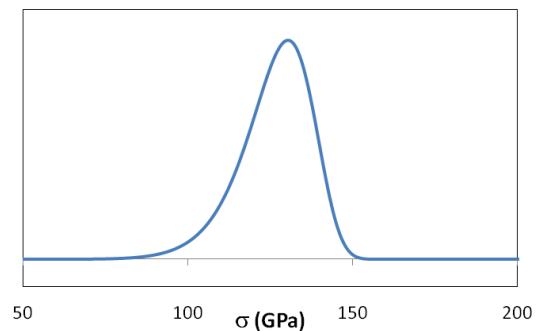


**Figure 1** Schematic representation of hierarchical scheme used in the HFBM model

### 3 Simulation results

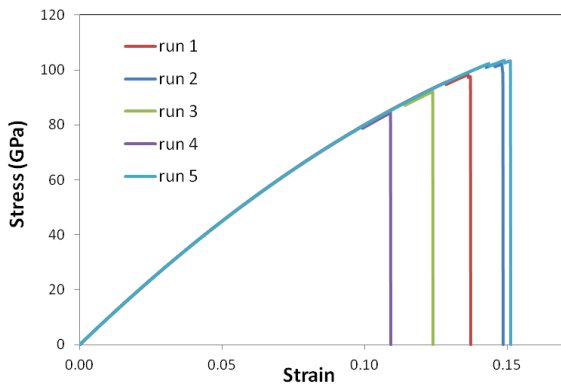
Two specific systems are considered in the following, namely graphene ribbon bundles/fibres, and graphene-reinforced polymer composites.

**3.1 Graphene ribbons/fibres** Graphene nanoribbons, derived from the unzipping of CNTs, were first studied by Kosynkin et al.[2]. We wish to theoretically numerically characterize the mechanical behaviour of nanoribbon bundles and evaluate the possible influence of defects on the overall response at microscale and macroscale. In order to do this, we use the parameters derived experimentally by Lee et al. [1] for single graphene sheets at level 1 of our HFBM. The resulting Weibull strength distribution for the graphene ribbons in the bundle is shown in Fig.2, corresponding to scale and shape parameters of  $\sigma_0=131$  GPa and  $m=14$ . The specimens are discretized with  $N_x=10^3$  and  $N_y=10^2$  fibres, and simulations are repeated  $10^3$  times to calculate mean values.



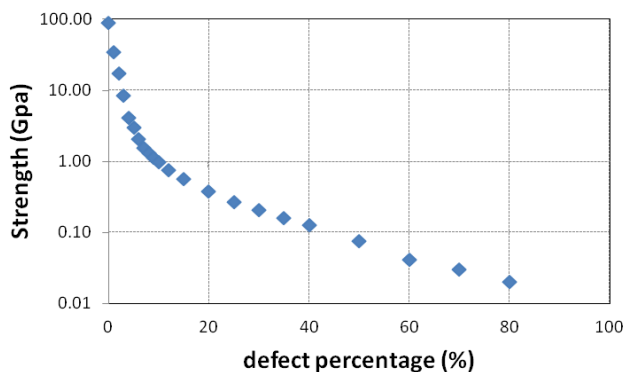
**Figure 2** Weibull strength distribution for single graphene ribbons.

Some typical output stress-strain curves for the graphene ribbon bundles are shown in Fig.3. The different curves correspond to separate runs, which differ due to the statistical variation in level 1 parameters. The nonlinear elastic constitutive law used from [1] is reflected in the observed nonlinear behaviour up to fracture. The obtained mean bundle strength is 91 GPa, showing how "upscaling" leads to a considerable strength decrease, even in the presence of defects. This is due to the statistical variation in the ribbon strengths in the bundle, so that their failure is not simultaneous, and the maximum stress value in simulations is reached only for a given percentage of surviving ribbons, giving a reduced strength value.



**Figure 3** Simulated stress-strain curves for a graphene ribbon bundle in repeated runs

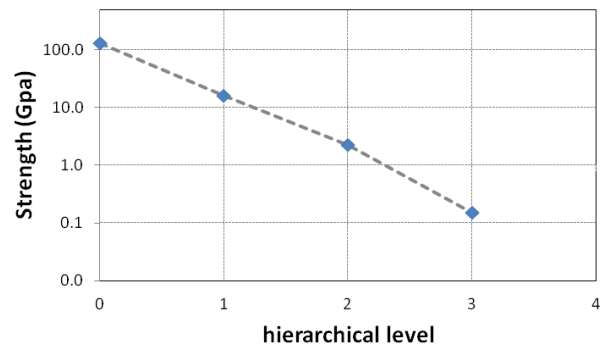
In addition to this effect, the role of defects is decisive in determining the overall strength of a graphene ribbon bundle. This can be verified by introducing randomly distributed “voids” in the array of fibres at single level in the model, with a set volume ratio (i.e. percentage). As expected, given the low-dimensionality of graphene, the presence of even small percentages of defects in the graphene ribbon bundles reduces the strength dramatically. Results are shown in Fig.4 in log scale: a 100-fold strength reduction is obtained for a defect percentage of approximately 10%.



**Figure 4** Strength decrease as a function of defect percentage

To compare these predictions with experimental values, we consider the data from Xu et al. [3] on graphene fibres. The fibre dimensions are length  $l=1$  m and radius  $r=20$  mm. Experimental results for tensile tests on these fibres yield strength values of approximately 140 MPa. To model this system, we use 3 hierarchical levels with  $N_x=N_y=100$  at each level, in order to span from micrometer dimensions to meters. Simulations are carried out for various defect percentages (uniformly distributed at all levels). An agreement with experimental values is obtained for a defect percentage of approximately 20%. Thus, it is possible to infer the actual defect percentage of the material, based on the measured mechanical properties, through numerical modelling. This result of a very high defect content is in keep-

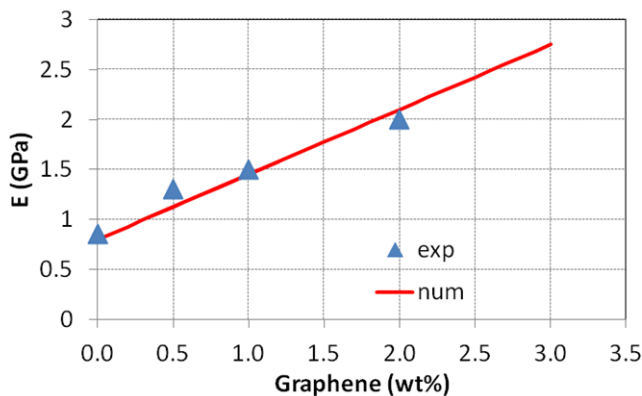
ing with the analysis in [3] whereby the “mechanical properties of the fibres can be greatly improved by optimization of the spinning process and post annealing to decrease the voids”. Numerical results for the determined defect percentage of 20% are reported in Fig.5, and show a power law-type decrease in the predicted strength with increasing hierarchical level, and therefore size.



**Figure 5** Strength decrease for a graphene fibre as a function of hierarchical level for a defect percentage of 20%.

### 3.2 Graphene-PVC composites

The second graphene-based system we consider is a graphene-reinforced Polyvinyl chloride (PVC) composite. Experimental data exist in the literature on this system which is of interest due to its flexibility, conductivity, high mechanical strength and thermal stability [13]. In particular researchers found that a significant enhancement in the mechanical properties of pure PVC films was obtained with a 2 wt.% loading of graphene, such as a 58% increase in Young’s modulus and an almost 130% improvement of tensile strength. HFBM simulations have been carried out on this system using for PVC a tensile strength of 25 MPa and Young’s modulus of 0.8 GPa, and considering increasing weight percentages of graphene fibres. Again, three hierarchical levels are used for the simulations. Numerical results are compared to experimental data in Fig.6, and very good agreement is found. A linear increase in Young’s modulus is found for increasing weight fractions of graphene, at least for small percentages, which is in the range of values that can be realized experimentally. For greater weight fractions, experimental stiffness values are found to saturate, probably due to the fact that an imperfect dispersion of graphene is obtained in the polymeric matrix, however this effect cannot be captured by the present model.



**Figure 6** Stiffening effect for increasing graphene reinforcement weight concentrations in graphene-PVC composites (experimental data from [13])

#### 4 Conclusions

Graphene shows great promise in the fields of mechanics and materials science due to its exceptional properties, and may prove a valid alternative to CNTs, for example as a reinforcement in composites. The presented HFBM model provides a simple but highly predictive tool to simulate the mechanical behaviour of nanostructured hierarchical graphene-based materials. In particular, the influence of defects at various hierarchical levels can be evaluated in macroscopic graphene fibres, and proves to be a critical parameter, with realistic estimates at about 20% for some recently produced fibres [3]. As far as graphene-polymer composites are concerned, the graphene reinforcement is shown to be very effective in the stiffening and strengthening of PVC -matrix composite materials. In future, the presented HFBM can be used to evaluate the potential performance of graphene composites and design tailor made characteristics for specific applications.

**Acknowledgements** This work is supported by the ERC Ideas Starting Grant no. 279985 "BIHNSAM—Bio-Inspired Hierarchical Super Nanomaterials", which is gratefully acknowledged. Computational resources were provided by the Politecnico di Torino's DAUIN High Performance Computing Initiative (<http://dauin-hpc.polito.it>).

#### References

- [1] H. Chen, M.B. Müller, K.J. Gilmore, G. G. Wallace, D.Li. *Advanced Materials* **20**(18), 3557–3561 (2008)
- [2] Kosynkin DV, Higginbotham AL, Sinitskii A, Lomeda JR, Dimiev A, Price BK, Tour JM, *Nature* **458**, 872-876 (2009)
- [3] Z.Xu and C. Gao, *Nature Communications* **2**: 571 (2011).
- [4] X.Li, W. Cai, J. An, S. Kim, J. Nah, D.Yang, R. Piner, A. Velamakanni, I. Jung, E. Tutuc, S. K. Banerjee, L. Colombo and R. S. Ruoff, *Science* **324** (5932), 1312-1314 (2009)
- [5] S.Bae, H.Kim, Y.Lee, X. Xu, J. Park, Y. Zheng, J. Balakrishnan, T. Lei, H.R. Kim, Y. Il Song, Y.-J. Kim, K. S. Kim, B. Özyilmaz, J.-H. Ahn, B. H. Hong and S. Iijima, *Nature Nanotechnology* **5**, 574–578 (2010).

- [6] S.Stankovich1, D.A. Dikin, G.H. B. Dommett, K.M. Kohlhaas, E.J. Zimney, E.A. Stach, R.D. Piner, S.T. Nguyen and R. S. Ruoff, *Nature* **442**, 282-286 (2006)
- [7] C. Lee, X. Wei, J. W. Kysar and J. Hone, *Science* **321**, 385-388 (2008).
- [8] N. M. Pugno, *International Journal of Fracture*, **140**, 158 2006.
- [9] N.Pugno, F.Bosia, A.Carpinteri, *Small* **4** (8), 1044–1052 (2008)
- [10] F.Bosia, M.Buehler, N.M.Pugno, *Physical Review E* **82**, 056103 (2010)
- [11] F.Bosia, N.M.Pugno, A. Carpinteri, *International Journal of Solids and Structures* **45**, 5856-5866 (2008).
- [12] W.Weibull, *Journal of Applied Mechanics - Transactions ASME* **18**, 293–297 (1951).
- [13] S.Vadukumpully, J. Paul, N. Mahanta, S. Valiyaveettil, *Carbon* **49**, 198 –205 (2011).