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**This is the author's manuscript**

*Original Citation:*

*Availability:*

This version is available <http://hdl.handle.net/2318/1571192> since 2016-06-23T12:40:15Z

*Published version:*

DOI:10.1016/j.joen.2015.07.002

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# UNIVERSITÀ DEGLI STUDI DI TORINO

***This is an author version of the contribution published on:***

*Questa è la versione dell'autore dell'opera:*

Journal of Endodontics, 41(10): 1706-10, 2015

DOI: 10.1016/j.joen.2015.07.002

***The definitive version is available at:***

*La versione definitiva è disponibile alla URL:*

<http://www.sciencedirect.com/science/article/pii/S0099239915006317>

## **Micro-CT evaluation of ProTaper Next and BioRace shaping outcomes in maxillary first molar curved canals.**

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**Abstract word count: 219**

**Text word count: 2480**

**Tables/Figures: 1/2**

**Acknowledgements:** the authors would like to thank Dr. Nicola Sodini (Sincrotrone Trieste S.C.p.A) for his valuable support in Micro-CT analysis and Dr. Elisa Bottero (lecturers at the Department of Endodontics, University of Turin Dental School) for active cooperation. E. Berutti declares financial involvement (patent licensing arrangements) with Dentsply Maillefer for ProGlider instruments.

## Abstract

**Introduction:** The aim of this micro-CT study was to describe the shaping properties of ProGlider/ProTaper Next (PG/PTN) and ScoutRace/BioRace (SR/BR) NiTi rotary systems.

**Methods:** Thirty maxillary first permanent molars were selected. Mesio-buccal canals were randomly assigned (n=15) to PG/PTN or SR/BR groups. Irrigation was performed with 5% NaOCl and 10% EDTA. Specimens were scanned (voxel size 9.1  $\mu\text{m}$ ) for matching volumes and surface areas and post-treatment analyses. Root canal centering ability, canal geometry enlargement and thickness of dentinal wall at inner curvature were assessed at apical level (A) and point of maximum curvature (C). Results were analyzed with four one-way ANOVAs. **Results:** . Canal centering ability was superior in PG/PTN ( $P = 0.006$  at A;  $P = 0.025$  at C). PG/PTN demonstrated a more conservative increase of canal areas ( $P = 0.027$  at A;  $P = 0.038$  at C). Centrifugal increase in canal diameters did not significantly differ between groups ( $P = 0.65$  at A;  $P = 0.61$  at C). Inner dentinal wall thickness was less reduced with PG/PTN compared with SR/BR, with no statistical differences ( $P = 0.23$  at C;  $P = 0.89$  at A). PG/PTN shaping taper ranged between 6–7%. **Conclusion:** Neither system produced significant shaping errors in curved canals. PG/PTN system showed better preservation of canal anatomy. PTN off-set section did not influence final preparation taper.

**Key words:** canal shaping, NiTi rotary instrument, micro-CT, ProTaper Next, BioRace, canal transportation

## Introduction

The introduction of nickel-titanium (NiTi) instruments has led to safer, easier and less invasive preparation of canals with preservation of the original canal anatomy (1, 2-7). The ProTaper Next (PTN) rotary system exhibits M-wire technology, whose properties allowed to reduce the number of instruments necessary to shape even extremely curved and narrow canals (6-11). The instruments are characterized by an off-set centered rectangular cross section that gives the files a characteristic swaggering motion during rotation. The taper of PTN instruments refers to the outer profile, not to the progression in section diameters. No data are available concerning the real post-shaping taper. Furthermore, the shaping ability of this system in curved canals has yet to be fully characterized. BioRace system (BR) is a widely diffused file manufactured from conventional austenite NiTi with a triangular cross section and NiTi electropolishing (12,13).

Micro-computed tomography (micro-CT) has emerged as a powerful tool for ex vivo evaluation of root canal morphology, being accurate as anatomical sectioning (14–18). Micro-CT enables analysis of volume changes, cross-sectional shape, taper and proportion of prepared surface by matching reconstructed sample volumes of pre- and post-operative canal systems (19,20). The primary objective of this ex vivo study was to describe shaping outcomes of PTN and BR systems in terms of volume and surface changes, canal centering ability and canal geometry modification by micro-CT analysis. The secondary objective was to quantify the effect of the swaggering motion on the resulting real taper after shaping with PTN.

## **Material and methods**

Maxillary first permanent molars extracted for periodontal disease were used in accordance with approval from the local ethics committee. Study power was set at 80% and a sample size of 15 specimens per group was calculated (G\*Power, Kiel University, Germany).

Low-resolution scout scans were performed (21) (450 projections through a 225° rotation, 100 kV, 80  $\mu$ A) to attain an overall outline of the root canal anatomy. COBRA 7.2 (Exxim, Pleasanton, CA, USA) software was used to reconstruct the axial slices with an isotropic voxel size of 36  $\mu$ m.

Reconstructed volumes were visualized with VGStudio MAX 2.0 software (Volume Graphics GMBH, Heidelberg, Germany). Morphological parameters of the mesio-buccal (MB1) canals were obtained. MB1 canals  $12 \pm 2$  mm from canal orifice to apical foramen,  $25^{\circ}$ – $40^{\circ}$  primary root curvature according to the Schneider method (22),  $4 < r \leq 8$  mm radius of curvature (23), and a point of maximum curvature located within the middle third of the root canal were utilized. Teeth with a distinct fourth canal orifice were selected and those with significant calcifications were excluded.

### **X-ray micro-CT analysis**

The selected samples were then scanned at higher spatial resolution (2400 projections through a  $360^{\circ}$  rotation, 100 kV, 80  $\mu$ A). Axial slices were reconstructed with COBRA 7.2 and elaborated for ring artifact reduction by the Pore3D software library (21). Reconstructed axial slices were equalized and converted to TIFF file format with ImageJ (NIH, Bethesda, MD) with an isotropic voxel size of 9.1  $\mu$ m . Each image stack was processed by Amira 5.3.3 (Visage Imaging, Richmond, Australia) for volume registration and cutting plane selection which was the same for pre- and post-treatment samples.

Each root canal path was analysed with high-resolution 3D rendering and orthogonal cross sections. Pre-operative root canal surface area and volume were collected. Root sections orthogonal to the canal axis were set at two different levels: 1 mm from the canal apex (A) and at the point of maximum curvature (C). Axial slices were analyzed with ImageJ to measure area and diameters (major and minor), using a minimum threshold algorithm (MT) to avoid manual errors (24). The major diameter was calculated as the distance between the two most distant pixels included in the root canal cross sectional area, the minor diameter was defined as the longest chord orthogonal to the respective major diameter (25). Measurements were made by an expert operator who was blind to allocation of specimens .

Final shaping taper of PTN was examined using high-resolution 3D rendering(Fig.2). Root sections orthogonal to the canal axis were set with a 1 mm step from apical foramen to canal orifice and minor diameters were measured.

### **Specimen preparation**

Forty-five teeth were assessed and 11 were excluded due to their anatomical features.. The remaining 34 teeth were randomly allocated to experimental groups, ProGlider and ProTaper Next (PG/PTN) and ScoutRace and BioRace (SR/BR), and between two expert operators using a computer-generated randomization table. Operators were experienced in both techniques and previously calibrated for pecking speed and pressure on the handpiece. Instruments in both groups were used with in and out motion, with no intentional brushing action against canal walls. As each instrument required a specific technique it was not possible to blind operators to their allocation. However, randomization, allocation and statistical analysis were performed by blinded operators. Following access cavity preparation, canal scouting was performed in all specimens with a #10 k-file at WL using Glyde™ (Dentsply Maillefer, Ballaigues, Switzerland) as lubricating agent (0.80 mg) (26). WL was established under 10X magnification (OPMI Pro Ergo, Carl Zeiss, Oberkochen, Germany) when the tip was visible at the apical foramen.

Two specimens from each group requested different preflaring and glide path protocols to reach full WL due to their anatomy and were excluded from the study.

In group PG/PTN (n=15), glide path was performed with ProGlider (PG) single file (0.16,.02 to .085) (Dentsply Maillefer, Ballaigues, Switzerland), using X-Smart motor (Dentsply Maillefer, Ballaigues, Switzerland) (300 rpm, 4 Ncm) at WL. Root canal shaping was performed with PTN X1 (0.17,.04 to .075) and X2 (0.25,.06 to .07) (Dentsply Maillefer, Ballaigues, Switzerland), using X-Smart (300 rpm, 4 Ncm) at WL.

In group SR/BR (n=15), glide path was performed with ScoutRace (SR) system (SR1, 2 and 3, taper .02 and tip size 0.10–0.15–0.20 mm, respectively) (FKG, La Chaux-de Fonds, Switzerland),

using X-Smart (600 rpm, 1.5 Ncm) at WL. Root canal shaping was performed with BR1 (0.15,.05), BR2 (0.25,.04) and BR3 (0.25,.06) (FKG, La Chaux-de Fonds, Switzerland), using X-Smart (600 rpm, 1 Ncm) at WL. New sets of instruments were used for each canal in both groups. The duration of instrumentation was recorded for each group.

Irrigation was performed with a 30G needle syringe and alternated 5% NaOCl with 10% EDTA, for a total of 10 ml each per specimen (27, 28). Root canals were dried with sterile paper points and specimens were micro-scanned for post-treatment analysis.

The following parameters were measured both in pre- and post-operative scans:

- root canal volume and surface area
- canal gravity center coordinates and shift in mm (to assess root canal centering ability); the center of each section was automatically segmented using ImageJ software before and after instrumentation through the center of mass algorithm and average canal transportation ( $d_c$ ) was calculated;
- ratio of diameter ratios (RDR) and ratio of cross-sectional areas (RA) (to assess symmetrical enlargement of the canal geometry) (15); RDR values closer to 1 correspond to a better maintenance of the original canal geometry; the ratio of cross-sectional areas (RA) quantifies the tendency of the instrument to enlarge the root canal space and values closer to 1 correspond to a reduced enlargement;
- thickness of dentinal wall at inner curvature to evaluate the percent of dentin removal after instrumentation ( $d_{inn}$ ).

Parameters were measured at A and C levels of analysis. Shapiro-Wilk normality test was used to analyze data distribution.

Four one-way factorial ANOVAs ( $P < 0.05$ ) were performed to evaluate the influence of instrumentation on RDR, RA,  $d_c$  and  $d_{inn}$  at each level of analysis (A and C). Fisher's Least

Significance Difference procedure was utilized as a post-hoc test. All statistical analyses were performed with Minitab 15 software package (Minitab Inc., State College, PA, USA).

## Results

No instrument fractured during canal preparation. Initial mean canal surface areas were 16.611 mm<sup>2</sup> and 16.004 mm<sup>2</sup> ( $P = 0.52$ ), initial mean canal volumes were 2.091 mm<sup>3</sup> and 1.934 mm<sup>3</sup> ( $P = 0.64$ ) in PG/PTN and SR/BR groups, respectively. Statistics of number of pecking motions and time, post-instrumentation canal surface and volume delta values, d\_c, RDR, RA, and d\_inn at A and C levels of analysis are represented in Table 1.

Fig.1 represents an example matching of pre-operative (green) and post-operative shapes (red) in both groups.

Canal centering ability (d\_c) was significantly superior in PG/PTN compared with SR/BR ( $P = 0.006$  at A;  $P = 0.025$  at C).

Both systems demonstrated a homogeneous increase in root canal diameters (RDR) at the points of analysis in each direction ( $P = 0.65$  at A;  $P = 0.61$  at C). PG/PTN demonstrated a more conservative enlargement of the root canal areas (RA) at both points of analysis compared to SR/BR ( $P = 0.027$  at A;  $P = 0.038$  at C).

On average, PG/PTN reduced the inner dentinal wall thickness (d\_inn) at C (-11.2%) to a lesser extent than SR/BR (-17.96%). However this was not statistically significant ( $P = 0.23$ ). No differences were found between groups at A ( $P = 0.89$ ).

A 3D visualization of a root canal shaped with PG/PTN and SR/BR systems (red) and the shaping outcomes are presented in Fig.2 a–c. Progression of root canal diameters (1 mm step) from the apical foramen to root canal orifice demonstrates that the real shaping taper ranges from 6–7% in

the PG/PTN group, coherent with the declared taper of the instrument profile.

## **Discussion**

Previous studies have shown that root canal transportation leads to excessive dentine removal, with a high risk of straightening the original canal curvature and ledge formation with less residual thickness of the dentine walls, significantly affecting long term prognosis (29–31). Evaluation of changes to canal shape post-instrumentation is a reliable assessment of the ability of a shaping technique to preserve the original anatomy (3, 9). Studies have demonstrated the value and reproducibility of micro-CT when evaluating shaping outcomes after preparation with different NiTi instruments (15–20). This *ex vivo* study used micro-CT to describe the shaping performances of the PTN and BR systems in curved root canals, following glide path with PG and SR, respectively. Previous studies demonstrated that canal transportation was more pronounced when shaping narrow curved canals than wider canals of maxillary molars (26). Therefore, MB1 root canals were selected. Natural variation in morphology has led to the establishment of measures to ensure comparability of pre-instrumentation geometric parameters (9, 22). This study considered apical and maximum curvature levels of analysis, representing the areas where iatrogenesis and canal aberrations may be easily introduced (29).

Glide path and coronal enlargement are crucial to achieving a more direct path to the apical end of the canal, removing coronal interferences and reducing the number of pecking motions required to reach full WL (30, 32). Previous studies report that the creation of a glide path and preliminary enlargement enhances the performance of PTN instruments, while PTN without a glide path results in a higher mean volume of removed dentin (30, 33). PG reduced the stress in PTN X1 and pecking motions required during shaping due to its ability to create a preliminary flaring of the coronal and middle portions of the root canal (30, 33).

The PTN off-centered rectangular cross section gives the file a reduced pattern of contact between the instrument and canal wall(11, 34), providing the swaggering motion during instrument rotation. This feature has been suspected to change instrument envelope of motion, dramatically increasing the final taper of the preparation. The BR system, with a triangular cross-section design and alternating cutting edges, is a validated method with a centered section and a traditional NiTi alloy (10) and shows significantly different characteristics to PTN in terms of instrument design, number of files in the sequence, protocol of use, and duration of instrumentation. Besides instrument dimension, other factors including metallurgical properties, instrument design, kinematic and instrument use, may influence canal transportation (1, 7). The primary aim of this study was to assess canal preparation outcomes of two NiTi rotary systems with equal size and taper (#25, .06) at tip level, but different design and sections. Intentional brushing movement was avoided in both systems in order to eliminate operator-related parameters that are difficult to standardize and which may influence the final taper of the preparation, even inside the same tested group (35). No significant differences in post-instrumentation volumes and surface areas were recorded between groups. However, at both A and C, the lowest canal transportation scores were recorded with PG/PTN. Centrifugal increase in canal diameters did not significantly differ between groups (RDR), while PG/PTN demonstrated a more conservative increase of canal areas (RA) and reduction of the inner dentinal wall thickness at point of maximum curvature, probably due to the reduced number of instruments and duration of instrumentation.

The secondary objective of this study was to describe the real final taper of the PG/PTN system root canal preparation. Thus, the analysis aimed to assess the influence of instrument off-set section, swaggering movement and variable taper on the real final taper of the preparation which was compared with the declared taper of the final shaping instrument (PTN X2). In this study, 3D analysis of the final taper after shaping with PTN X2 demonstrated a homogenous increase in canal taper, ranging from 6–7%, coherent with the declared taper of the instrument profile.

In conclusion, within the limits of this study, both SR/BR and PG/PTN shaping systems provided root canal preparation without significant shaping errors in maxillary first molar curved canals. The PG/PTN system resulted in a more centered and less invasive preparation. The offset section and swaggering motion of PTN did not appear to enlarge the root canal more than the declared taper of the instrument.

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## Figure legends

**Fig. 1:** Representative images of matching 3D reconstructions for PG/PTN (A) and SR/BR (B) groups. *Green* indicates the pre-operative volume and *Red* indicates the post-operative volume.

**Fig. 2:** Representative images of ProTaper Next and BioRace post-shaping taper. 3D reconstruction with 1 mm step cutting planes (a); images of corresponding axial slices (b) and descriptive statistics of the minor canal diameters for each slice and relative percentage taper of each step (c).

## Table legends

**Table 1:** shaping and 3D/2D parameters (Mean  $\pm$  SD) utilized for post-instrumentation analysis in each group (PG/PTN = ProGlider/ProTaper Next; SR/BR = ScoutRace/BioRace). Points of analysis: M = maximum curvature; A = 1 mm from apical foramen; RDR = ratio of diameters ratio; RA = ratio of cross-sectional areas; d\_c = average canal transportation by center of gravity shift; d\_inn = percentage of dentin thickness removal at inner curve.

**Table 1:** shaping and 3D/2D parameters (Mean±SD) utilized for post- instrumentation analysis in each group (PG/PTN = ProGlider/ProTaper Next; SR/BR = ScoutRace/BioRace). Points of analysis: M = maximum curvature; A = 1 mm from apical foramen. RDR= ratio of diameters ratio; RA= ratio of cross-sectional areas; d\_c = average canal transportation by centre of gravity shift; d\_inn = percentage of dentin thickness removal at inner curve

Group	Pecking motions	Shaping time (sec)	$\Delta$ volume (mm <sup>3</sup> )	$\Delta$ surface area (mm <sup>2</sup> )	Level of analysis	RDR	RA	d_c (mm)	d_inn (%)
PG/PTN	15.4±1.9 <sup>a</sup>	32.6±4.9 <sup>a</sup>	0.76±0.4	2.81±1.3	M	0.86±0.12	1.53±0.48 <sup>a</sup>	0.05±0.03 <sup>a</sup>	11.20±10.39
					A	0.93±0.08	1.40±0.37 <sup>a</sup>	0.03±0.02 <sup>a</sup>	8.81±8.11
SR/BR	21±2.8 <sup>b</sup>	36.6±3.5 <sup>b</sup>	0.88±0.31	3.06±0.9	M	0.91±0.30	2.23±1.02 <sup>b</sup>	0.09±0.05 <sup>b</sup>	17.96±15.96
					A	0.90±0.27	2.01±0.89 <sup>b</sup>	0.06±0.03 <sup>b</sup>	8.41±7.78

Different superscript letters in the same column indicate significant differences between groups ( $P < 0.05$ ). For 2D parameters (RDR, RA, centre of gravity shift, percentage reduction in thickness values) significance was compared for the same level of analysis (M=maximum curvature or A=apical).