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# Synthesis and Characterization of Thermoelectric $\text{Co}_2\text{XSn}$ ( $\text{X} = \text{Zr}, \text{Hf}$ ) Heusler Alloys

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**Abstract:** In this work, we report the results of an experimental investigation on the synthesis, structure, microstructure, mechanical, electrical conductivity, and Seebeck coefficient of  $\text{Co}_2\text{XSn}$  ( $\text{X} = \text{Zr}, \text{Hf}$ ) alloys. In both the alloys, the main constituent is a full Heusler-type compound that coexists with small amounts of secondary phases. Both alloys show a rather high Vickers hardness (around 900 HV) and an indentation fracture toughness typical of ceramics (around  $2 \text{ MPa}\cdot\text{m}^{1/2}$ ). The electronic transport properties of the two alloys were measured for the first time. The temperature dependence of both the Seebeck coefficient and the electrical conductivity of the two alloys shows a change in correspondence of the Curie temperature. The Seebeck coefficient reaches a constant plateau, while the electrical conductivities show a transition from metallic to semiconductor behavior. As a consequence, almost constant values of the power factor have been obtained for the power factor above the Curie temperature, which is promising for an efficient exploitation of thermal gradients of several hundreds of degree in waste heat harvesting applications. Finally, on the basis of results from this work and from the literature, the effect of the substitution of the X element on the electronic transport properties in the series  $\text{Co}_2\text{XSn}$  ( $\text{X} = \text{Ti}, \text{Zr}, \text{Hf}$ ) is discussed.

**Keywords:** Heusler; arc melting; Seebeck; electrical conductivity; thermoelectric; Curie temperature

## 1. Introduction

The Heusler alloys represent an important class of thermoelectric materials since they generally combine good performances with high thermal stability, and, in most cases, ease of synthesis. The structure of the full-Heusler (FH) compounds consists of 4 FCC sublattices with a  $\text{L}2_1$ -type structure, while the one of the half-Heusler (HH) compounds consists of 3 FCC sublattices arranged according to the C1b lattice prototype [1]. On the one hand, HH alloys show remarkable  $zT$  values such as 1.5 for  $(\text{Zr}_{0.5}\text{Hf}_{0.5})_{0.5}\text{Ti}_{0.5}\text{NiSn}_{0.998}\text{Sb}_{0.002}$  [2] and  $\text{Nb}_{0.88}\text{Hf}_{0.12}\text{FeSb}$  [3], and about 1.2 for  $\text{Ti}_{0.5}\text{Zr}_{0.5}\text{NiSn}_{0.98}\text{Sb}_{0.02}$  [4] and densification-aided  $\text{Ti}_{0.5}\text{Zr}_{0.5}\text{NiSn}$  [5]. On the other hand, FH alloys exhibit numerous worthwhile properties related to their particular electronic structures. For example, Co-based FH alloys are proved to be half-metallic ferromagnets, and they display an electronic density of states (DOS), which leads to the manifestation of spin-Seebeck effects [6–8]. For this reason, the Co-based full-Heusler compounds can be promising materials for application in spintronics and spin-caloritronics [7,9–11].

One of the first investigation on Co-based FH alloys was the work of Ziebeck and Webster [12] in 1974, where both the structural characterization by means of neutron diffraction and the magnetic properties are reported. Later, in 1987, De Souza et al. [13] confirmed the magnetic properties reported

in Ref. [12]. Furthermore, they reported a Curie temperature ( $T_C$ ) of 460 K for  $\text{Co}_2\text{ZrSn}$  and 423 K for  $\text{Co}_2\text{HfSn}$ .

As far as the thermoelectric properties are concerned, Barth et al. [14] investigated the magnetic and electronic transport properties of the  $\text{Co}_2\text{TiZ}$  ( $Z = \text{Si, Ge, Sn}$ ) alloys and reported a maximum value of thermopower of about  $-50 \mu\text{V/K}$  (which is quite high for a metallic compound) together with a  $T_C$  of 360 K for the  $\text{Co}_2\text{TiSn}$  alloy. Moreover, they highlighted that a remarkable characteristic of these materials is the fact that the absolute value of the Seebeck coefficient linearly increases up to  $T_C$ , and then it settles in a plateau and remains constant throughout the entire analyzed range of temperature. They suggested also that this anomalous trend of the Seebeck coefficient can be explained by the half-metallic behavior of the Co-based family of FH alloys. Concerning the electrical conductivity ( $\sigma$ ),  $\text{Co}_2\text{TiSn}$  exhibits a relatively small value of 2851 S/cm after  $T_C$ , which is the smallest of all compounds investigated in that work.

It is also important to mention that the band structures and the electronic DOS of the  $\text{Co}_2\text{XSn}$  (where X is a metal of group 4 of the periodic table, namely Ti, Zr, and Hf) alloys have been studied in several theoretical investigations [6–9,15–17]. There is a general agreement on the fact that all the three alloys show an electronic DOS typical of half-metallic ferromagnets. This particular property manifests itself in magnetic compounds with an electronic DOS consisting in quite continuous majority-spin sub-bands and minority-spin sub-bands that instead exhibit semiconductor-like band gaps [6]. This property would allow these compounds, at least below  $T_C$ , to generate spin-Seebeck effects [6–9], which can be described as the ability of a material to conduct spin-polarized electrons when the system is subjected to thermal gradients [7,10]. Despite these promising properties, until now, there have been no significant advances in the determination of the transport properties of the  $\text{Co}_2\text{XSn}$  compounds.

On the one hand, mechanical properties are useful for evaluating the reliability of materials when assembled in a thermoelectric module. On the other hand, since the understanding of the thermoelectric properties of the Co-based FH alloys is still lacking, it is valuable to gather as much information as possible on the behavior of these compounds in view of spintronic and waste heat harvesting applications. Thus, the aim of this work is to measure for the first time the mechanical properties (i.e., Vickers hardness, indentation fracture toughness) and electronic transport properties (i.e., Seebeck coefficient, electrical conductivity) of the  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  alloys. Furthermore, considering the properties of the  $\text{Co}_2\text{XSn}$  ( $X = \text{Ti, Zr, Hf}$ ) series of FH alloys, it is discussed how the electronic transport properties may vary when the X metal is changed.

## 2. Materials and Methods

The pure elements were weighted in the appropriate stoichiometric quantities and melted in the arc furnace (Edmund Bühler GmbH, Bodelshausen, Germany). Due to the large difference in the melting points of Zr/Hf and Sn, two pre-alloys were synthesized for each FH system, namely CoZr and CoSn for  $\text{Co}_2\text{ZrSn}$ , and CoHf and CoSn for  $\text{Co}_2\text{HfSn}$ , to guarantee a better homogenization of the melt. Pre-alloys were melted together several times in order to obtain homogeneous samples. Then, the ingots were wrapped in tantalum foils, sealed in evacuated quartz tubes, and annealed at 800 °C for 6 days.

X-ray diffraction (XRD) investigation was performed in Bragg–Brentano configuration with a X'Pert Pro diffractometer (PANalytical B.V., Almelo, The Netherlands) using a Cu-K $\alpha$  radiation as the X-ray source. For the XRD analysis, the samples were crushed in thin powders to remove the effect of possible preferred crystallographic orientations. The Rietveld refinements of the XRD patterns were performed with the MAUD software [18]. The surface analysis was executed by Scanning Electronic Microscopy (SEM) with an EVO 50 microscope (Carl Zeiss Microscopy GmbH, Jena, Germany) equipped with an Inca Energy 250 Energy Dispersion Spectrometer (EDS) under vacuum of  $10^{-6}$  mbar, 20 kV of potential, and 150 pA of current. All the SEM images presented in this work were collected

in backscattered electrons (BSE) mode on mechanically polished surfaces. The XRD and SEM-EDS investigations were performed on both the as-cast and annealed specimens.

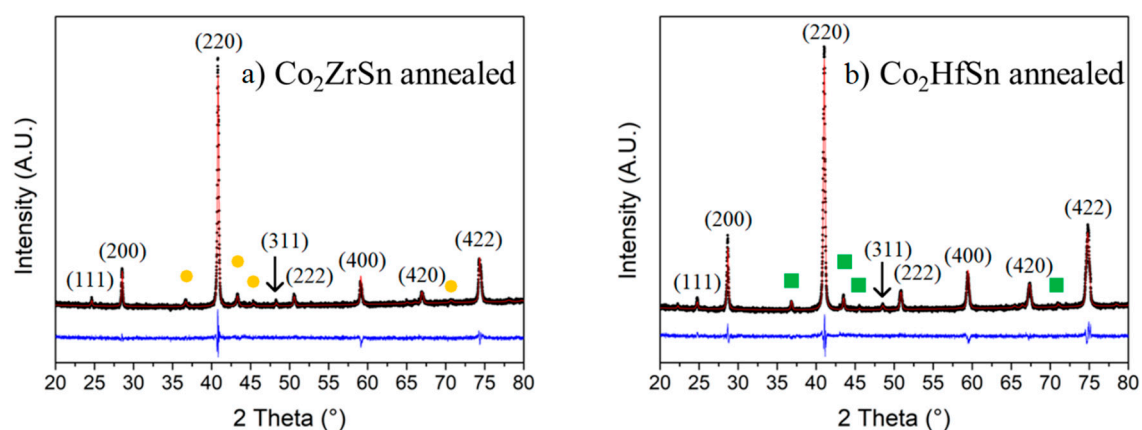
Microhardness measurements were performed on the annealed samples with a microhardness tester (Buehler, Lake Bluff, IL, USA) using a load of 4.9 N. The length of the indent diagonals and crack length were measured using a DMLM optical microscope (Leica, Wetzlar, Germany). The error associated with the mechanical properties was calculated using the standard t-student type formula for independent measurements, or  $Er = SDt/n^{1/2}$  (where  $Er$  is the obtained error,  $SD$  is the standard deviation,  $t$  is the tabulated t-student value relative to a confidence interval of 95%, and  $n$  is the number of independent measurements). The densities of the two alloys were measured by weighting ingots of known volume and by the Archimedes principle using a pycnometer.

The Seebeck coefficient and electrical conductivity were measured on bar-shaped annealed samples ( $12 \times 2 \times 2 \text{ mm}^3$ ) under He flow between room temperature and 778 K by using a custom test apparatus described in ref. [19]. Furthermore, in order to assess the thermal stability of the alloys, the properties were measured upon heating and cooling.

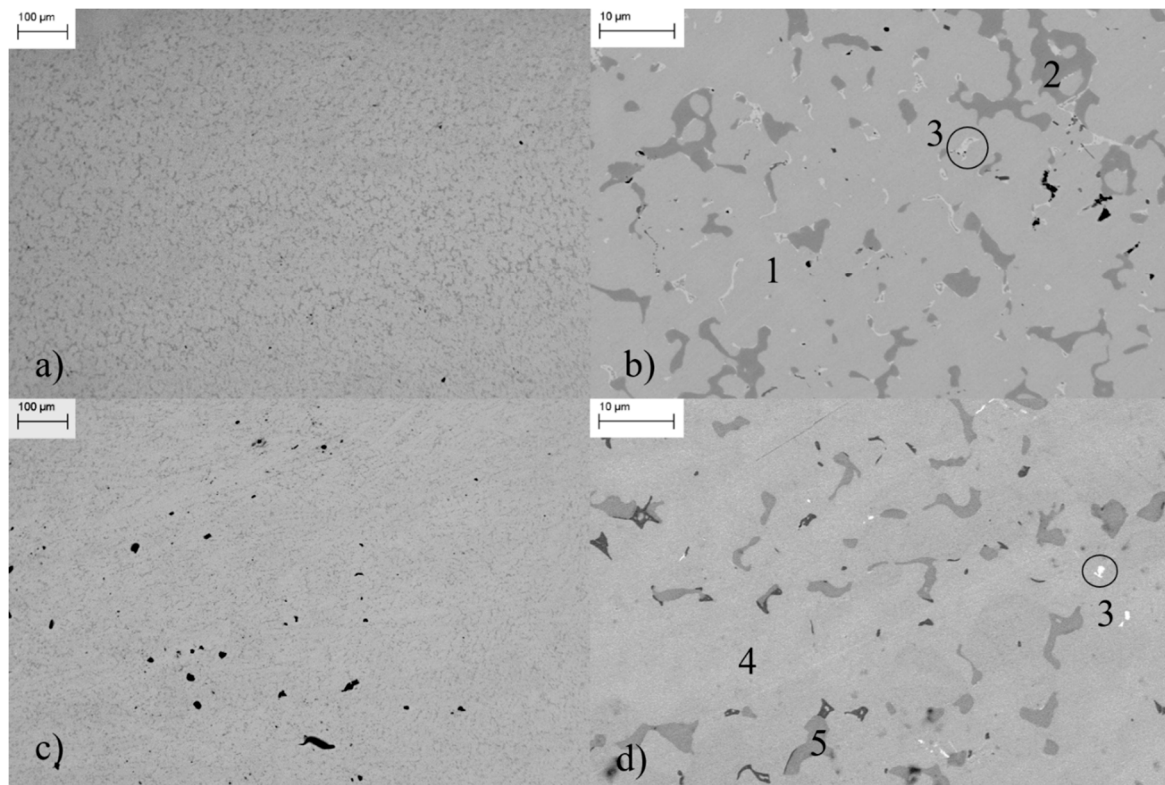
### 3. Results and Discussion

#### 3.1. Structural and Microstructural Characterization

The XRD patterns of both annealed alloys are shown in Figure 1. The XRD patterns of the as-cast alloys are shown in the supplementary materials (Figure S1). Figure 2a,b and Figure 2c,d show the backscattered SEM images of annealed  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  ingots, respectively, where the gray contrast suggests the homogeneous distribution of two secondary phases immersed in the main phase. The same SEM images relative to the as-cast alloys can be found in the supplementary materials (Figures S2 and S3). Table 1 shows the results of the Rietveld refinement of the XRD patterns shown in Figure 1 and the EDS elemental compositions of the phases observed in Figure 2, which are all related to the annealed samples, together with the results of the same investigations performed on the as-cast alloys. As reported in Table 1, both the Rietveld refinement and the EDS investigation indicate that phase 1 and 4 correspond to the  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  full Heusler structures, respectively, and they represent the main component of each alloy. In the case of  $\text{Co}_2\text{ZrSn}$  alloy, phases 2 and 3 are found to be the binary compounds  $\text{Co}_2\text{Zr}$  and  $\text{CoSn}$ , respectively. In the case of  $\text{Co}_2\text{HfSn}$  alloy, phases 3 and 5 are the binary compounds  $\text{CoSn}$  and  $\text{Co}_2\text{Hf}$ , respectively. In addition, Ziebeck and Webster [12] reported the presence of secondary phases, together with the FH phase even after annealing.



**Figure 1.** XRD patterns and Rietveld refinements of the  $\text{Co}_2\text{ZrSn}$  (a) and  $\text{Co}_2\text{HfSn}$  (b) annealed alloys. The black symbols and the red continuous line are the experimental and the calculated patterns respectively, while the blue line represents the difference between the two. The peaks proper of the full-Heusler phases are marked with their relative Miller indexes, whereas the signals of the secondary phases are highlighted with colored shapes (orange circles for  $\text{Co}_2\text{Zr}$  and green squares for  $\text{Co}_2\text{Hf}$ ).



**Figure 2.** Backscattered electrons SEM images of the  $\text{Co}_2\text{ZrSn}$  (a,b) and  $\text{Co}_2\text{HfSn}$  (c,d) annealed alloys. In accordance with the results of the Rietveld refinement of the XRD patterns (Figure 1 and Table 1), the observed phases are the  $\text{L}_{21}$ -type  $\text{Co}_2\text{ZrSn}$  full-Heusler (1), the C15-type  $\text{Co}_2\text{Zr}$  (2), CoSn (3), the  $\text{L}_{21}$ -type  $\text{Co}_2\text{HfSn}$  full-Heusler (4), and the C15-type  $\text{Co}_2\text{Hf}$  (5).

Average EDS measurements at low magnifications indicated that the overall composition of the specimens slightly deviates from the nominal stoichiometry. The average atomic compositions of the samples resulted to be 53% Co, 25% Zr, and 22% Sn for the  $\text{Co}_2\text{ZrSn}$  sample, and 51% Co, 25% Hf, and 24% Sn for the  $\text{Co}_2\text{HfSn}$  alloy, indicating slight Sn depletion and Co excess, with consequent formation of the observed secondary phases.

As reported in Table 1, the Rietveld analysis allowed quantifying the amount of secondary phases in the samples, which is 12% for  $\text{Co}_2\text{Zr}$  (2) and 7% for  $\text{Co}_2\text{Hf}$  (5). Concerning phase 3 (CoSn), its abundance is too small to be calculated with the Rietveld refinement (so its quantity will be considered negligible). The relative amount of the secondary phases does not change after annealing; however, slight changes of the EDS phase composition and lattice parameters can be observed. The lattice parameters found for the as-cast alloys are 6.2338 Å and 6.2101 Å for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$ , respectively. After annealing, the values of the lattice parameters become 6.2458 Å for  $\text{Co}_2\text{ZrSn}$  and 6.2157 Å for  $\text{Co}_2\text{HfSn}$ , which are very close to the equilibrium values reported by Ziebeck et al. [12] (i.e., 6.249 Å and 6.218 Å for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$ , respectively).

Densities of 9.2 g/cm<sup>3</sup> and 11.7 g/cm<sup>3</sup> were obtained for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  samples, respectively. As a result of the presence of secondary phases and the deviation of the phase composition from the stoichiometry (see Table 1), the measured values cannot be compared with the values of crystallographic density for the pristine compounds [20] (i.e., 8.92 g/cm<sup>3</sup> and 11.47 g/cm<sup>3</sup> for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$ , respectively), and experimental values [12] of monophasic  $\text{Co}_2\text{ZrSn}$  (8.90 g/cm<sup>3</sup>) and  $\text{Co}_2\text{HfSn}$  (11.40 g/cm<sup>3</sup>) [12]. Thus, the crystallographic density of each phase was calculated on the basis of the actual composition and the refined lattice parameter. Subsequently, the theoretical densities of the two-phases samples were obtained as the weighted average of the crystallographic density of the phases present in each sample, leading to values of 9.2 g/cm<sup>3</sup> and 11.9 g/cm<sup>3</sup> for the  $\text{Co}_2\text{ZrSn}$  and

Co<sub>2</sub>HfSn samples, respectively. It follows that the relative densities of Co<sub>2</sub>ZrSn and Co<sub>2</sub>HfSn samples are 100% and 98%, respectively.

**Table 1.** Composition, prototype–structure, cell parameters, and relative abundances of the different phases in the Co<sub>2</sub>ZrSn and Co<sub>2</sub>HfSn samples. The structure of the phase 3, CoSn, is shown as reported in the Co–Sn phase diagrams [21].

Co <sub>2</sub> ZrSn As-Cast							
Elemental composition (at %)			Label	Phase	Structure	a (Å)	Abundance (wt %)
Co	Zr	Sn					
45	28	27	1	Co <sub>2</sub> ZrSn	L2 <sub>1</sub>	6.2338	88%
65	21	13	2	Co <sub>2</sub> Zr <sub>x</sub> Sn <sub>y</sub>	C15	6.9174	12%
58	-	42	3	CoSn	B35	-	-
Co <sub>2</sub> ZrSn Annealed							
Elemental composition (at %)			Label	Phase	Structure	a (Å)	Abundance (wt %)
Co	Zr	Sn					
46	27	27	1	Co <sub>2</sub> ZrSn	L2 <sub>1</sub>	6.2458	88%
66	19	15	2	Co <sub>2</sub> Zr <sub>x</sub> Sn <sub>y</sub>	C15	6.9212	12%
58	-	42	3	CoSn	B35	-	-
Co <sub>2</sub> HfSn As-Cast							
Elemental composition (at %)			Label	Phase	Structure	a (Å)	Abundance (wt %)
Co	Hf	Sn					
45	27	28	4	Co <sub>2</sub> HfSn	L2 <sub>1</sub>	6.2101	93%
65	26	9	5	Co <sub>2</sub> Hf <sub>x</sub> Sn <sub>y</sub>	C15	6.9024	7%
56	-	44	3	CoSn	B35	-	-
Co <sub>2</sub> HfSn Annealed							
Elemental composition (at %)			Label	Phase	Structure	a (Å)	Abundance (wt %)
Co	Hf	Sn					
47	26	27	4	Co <sub>2</sub> HfSn	L2 <sub>1</sub>	6.2157	93%
66	25	9	5	Co <sub>2</sub> Hf <sub>x</sub> Sn <sub>y</sub>	C15	6.8915	7%
55	-	44	3	CoSn	B35	-	-

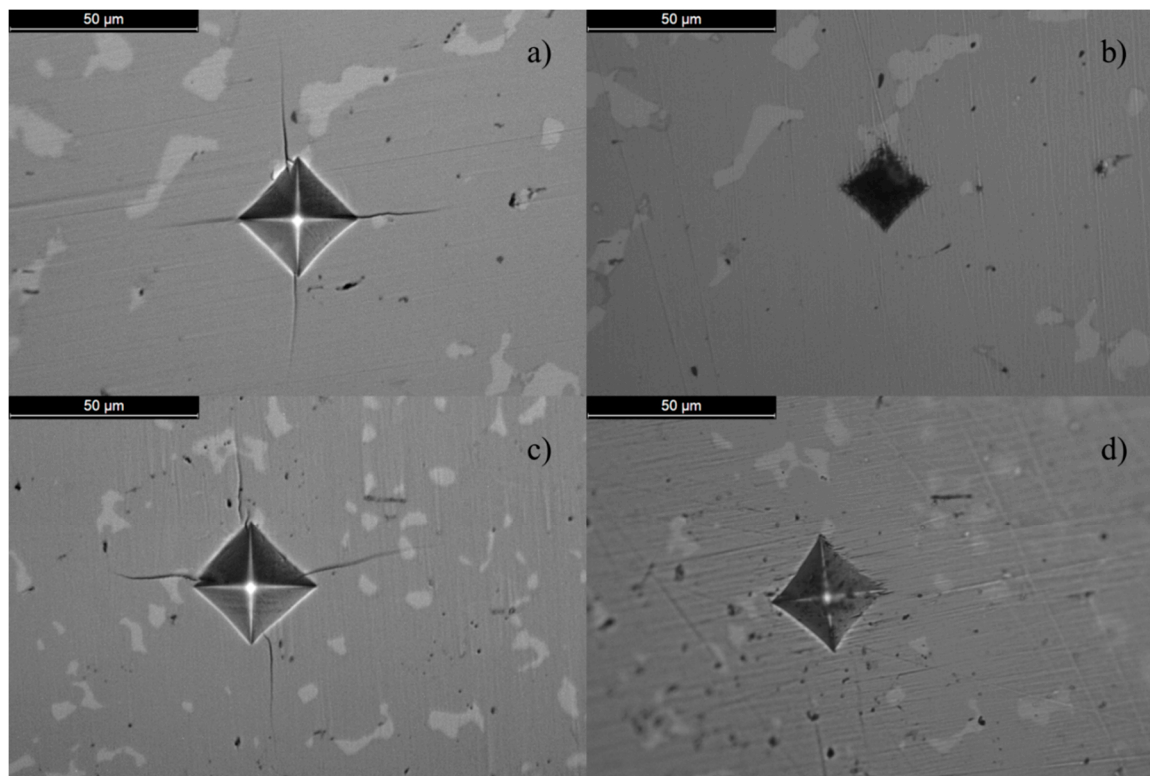
Ultimately, the unaltered relative abundance of the phases before and after the annealing treatment, and the small changes in their elementary composition and in the lattice parameters suggest that the full-Heusler phases 1 and 4 crystallize congruently from the melt with small impurities of secondary compounds Co<sub>2</sub>Zr and Co<sub>2</sub>Hf (2 and 5 respectively) and small traces of CoSn (3), which is due to the slight deviation of the prepared samples from the nominal stoichiometry. Thus, these alloys can be easily processed by direct solidification of the melt.

### 3.2. Mechanical Properties

As reviewed by Ponton et al. [22], when the surface of a material is indented, the cracks that propagate from the imprint can be of two different classes: halfpenny type and Palmqvist type. It is known that the halfpenny cracks propagate both on the surface (radial direction) and deeply below (median direction) the imprint. For this reason, they are also called radial-median cracks. Conversely, the Palmqvist type is shallower and includes cracks that do not propagate directly below the indentation, but only in the radial direction. It is possible to distinguish between the two typologies of cracks by performing a light polishing of the surface of the sample after indentation. After the procedure, if the cracks remain visible and always connected to the inverted pyramid of the indent, the behavior can be classified as halfpenny; whereas, a small detachment should be visible in case of cracks of the Palmqvist type, or, alternatively, only the indenter imprint should be observed in case of

very shallow cracks [23–25]. It was also generally observed that fairly shallow Palmqvist-type cracks are expected for hard metallic materials [23].

As expected, significant cracks have been observed after the first indentation, which has been used to determine the hardness, as reported in Table 2. After light polishing of the surface using a 3  $\mu\text{m}$  diamond paste, the radial cracks were no longer visible, indicating that these are extremely shallow. In Figure 3, as an example, one of the several indentations performed for each alloy is shown before and after the polishing treatment. No secondary cracks propagated from the Vickers imprint, which indicates that the whole load was transferred to the radial cracks, allowing an accurate estimation of the fracture toughness ( $K_{IC}$ ). The same result was observed for all the other indentations.



**Figure 3.** Examples of Vickers indentations on the  $\text{Co}_2\text{ZrSn}$  (panel **a** and **b**) and  $\text{Co}_2\text{HfSn}$  (panel **c** and **d**) alloys before (**a,c**) and after (**b,d**) light polishing.

Several polishing cycles were performed until the Vickers imprints disappeared (not shown), and also in these cases, no median cracks were observed.

It is possible to distinguish between the two types of cracks from the ratios  $c/a$  or  $l/a$  (where  $c$  is the length of the cracks from the center of the indent to their tip,  $a$  is half of the indentation diagonal, and  $l$  is the length of the crack measured from the corner of the indent). Being  $c = a + l$ , it turns out that  $c/a$  and  $l/a$  are linked by the following relationship  $l/a = (c/a) - 1$ . According to Refs. [23] and [26], when  $c/a \leq 2.5$  (or  $l/a \leq 1.5$ ), the crack should be classified as Palmqvist. Other studies [27,28] fix the upper limit of Palmqvist cracks for values of  $l/a$  around 2.5 (or  $c/a \leq 3.5$ ). The  $l/a$  ratio was calculated for both the alloys and the values obtained are lower than 1.5 in all the cases (see Table 2).

Therefore, in agreement to the micrographic observations, the cracks can be described as Palmqvist-type, so the fracture toughness  $K_{IC}$  can be evaluated using the Shetty–Wright–Mincer–Clauer equation [22,29], which in the case of a standard Vickers indenter is

$$K_{IC} = 0.0319 \cdot \frac{P}{a \cdot l^{1/2}} \quad (1)$$

where  $P$  is the applied load.

As reported in Table 2, the two alloys exhibit similar mechanical properties, showing a rather high hardness for metallic compounds and a fracture toughness comparable to those of ceramics [30]. These values are close to those generally exhibited by half Heusler alloys [31], so they can be considered suitable for application in devices.

**Table 2.** Average values of  $l/a$  ratios, Vickers hardness, and fracture toughness  $K_{IC}$  for the  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  alloys.

Alloy	Hardness (HV)	$l/a$	$K_{IC}$ ( $\text{MPa}\cdot\text{m}^{1/2}$ )
$\text{Co}_2\text{ZrSn}$	$903 \pm 31$	1.42	$2.07 \pm 0.23$
$\text{Co}_2\text{HfSn}$	$899 \pm 26$	1.41	$2.06 \pm 0.14$

### 3.3. Temperature Dependence of Electrical Conductivity, Seebeck Coefficient, and Power Factor

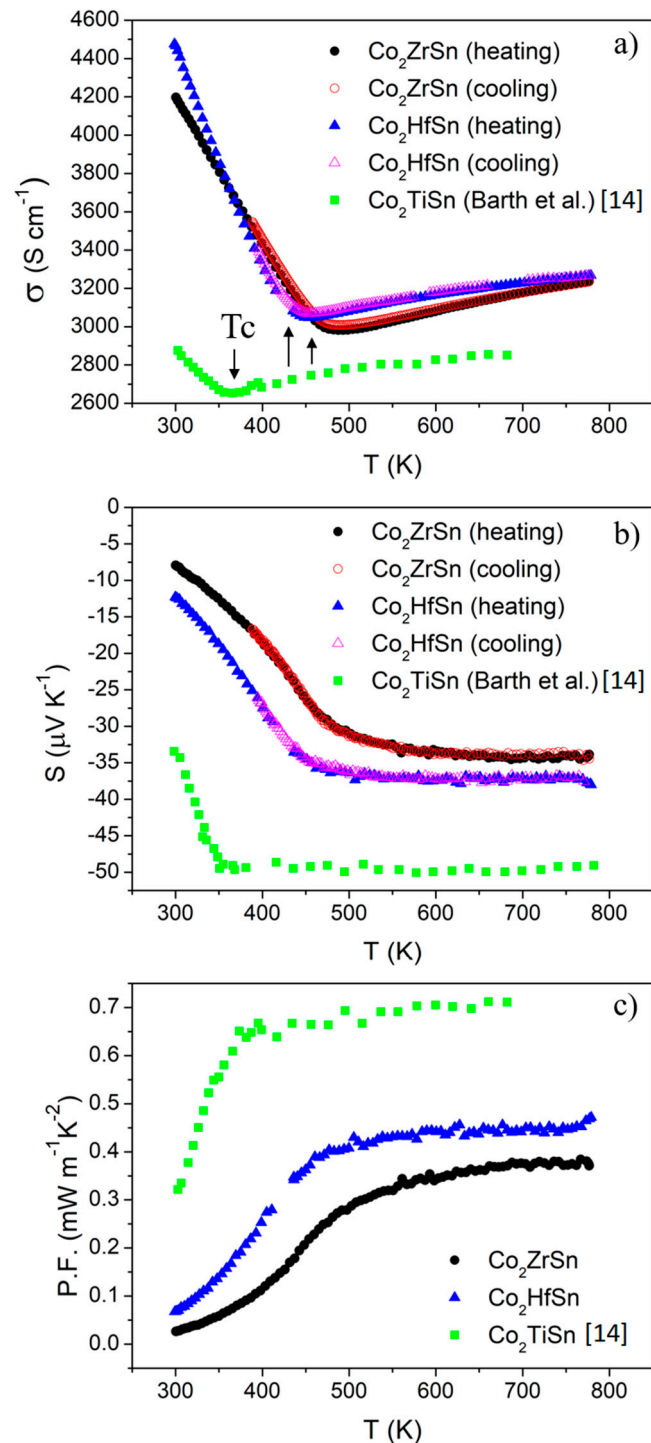
The trends of the electrical conductivity ( $\sigma$ ), Seebeck coefficient ( $S$ ), and power factor (PF) of annealed  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  ingots as a function of the temperature are shown in Figure 4. The transport properties were measured imposing a cyclic ramp of temperature in order to ensure the thermal stability of the samples and the reproducibility of the results under thermal cycling. Since no hysteresis is observable between heating and cooling, it is confirmed that the specimens are stable and the outputs are reproducible. Values previously obtained for  $\text{Co}_2\text{TiSn}$  [14] are reported for comparison. It should be noted that the values measured in this work refer to samples containing metallic secondary phases (i.e.,  $\text{Co}_2\text{Zr}$  and  $\text{Co}_2\text{Hf}$ ) [32], which likely tend to increase the electrical conductivity and lower the absolute value of the Seebeck coefficient with respect to the corresponding single-phase materials.

Figure 4a shows that the electrical conductivities of  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  are quite similar to each other. At room temperature (298 K), electrical conductivities values of 4196 S/cm and 4476 S/cm are measured for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$ , respectively. Since for this class of compounds, the Curie point can be determined measuring the point at which  $\sigma$  changes its slope [14],  $T_C$  values of 465 K and 426 K have been obtained for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$ , respectively. The electrical conductivity decreases almost linearly as a function of the temperature until  $T_C$  is reached, where it exhibits the lowest value, namely 2982 S/cm for  $\text{Co}_2\text{ZrSn}$  and 3046 S/cm for  $\text{Co}_2\text{HfSn}$ . After  $T_C$ , the electrical conductivities show a slight increase with the temperature, until values of 3235 S/cm and 3267 S/cm are observed for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$ , respectively, at 778 K. Considering these trends, it is possible to observe that the materials show metallic-like behavior at temperatures lower than  $T_C$ , whereas the electrical conductivities switch to a semiconductor-like behavior at higher temperatures. This is a consequence of the ferromagnetic–paramagnetic transition, which strongly influences the electronic DOS of the alloys. These results are in good agreement with those reported by De Souza et al. [13]

The Seebeck coefficient of both alloys is shown in Figure 4b as a function of temperature. It is negative as in the case of  $\text{Co}_2\text{TiSn}$  [14], indicating that the major charge carriers are electrons (n-type). At 298 K, the values of  $S$  are  $-9 \mu\text{V/K}$  and  $-13 \mu\text{V/K}$  for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  alloys, respectively. The absolute values of  $S$  of two alloys show a linear increase from room temperature to  $T_C$ . At higher temperatures, the values of  $S$  settle on a plateau at approximately  $-34 \mu\text{V/K}$  and  $-38 \mu\text{V/K}$  for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  samples, respectively. As reported for  $\text{Co}_2\text{TiSn}$  and other types of compounds [14,33,34], a linear increase of Seebeck coefficient followed by a constant value above the Curie temperature can be related to a steady position of the Fermi level over an extended range of temperature.

The behavior of the power factor ( $\text{PF} = S^2\sigma$ ) as a function of temperature is similar for the two alloys, as shown in Figure 4c. Between room temperature and  $T_C$ , the PF of the two alloys increases as a function of temperature. Above  $T_C$ , the PF values for both alloys reach a plateau, which is maintained up to 778 K. The observed behavior strongly reflects the trend of the Seebeck coefficient, which actually gives the main contributions to PF. At room temperature, values of  $0.026 \text{ mW}\cdot\text{m}^{-1}\cdot\text{K}^{-2}$  and  $0.068 \text{ mW}\cdot\text{m}^{-1}\cdot\text{K}^{-2}$  are observed for  $S$ , while at 778 K, they show a plateau value of  $0.38 \text{ mW}\cdot\text{m}^{-1}\cdot\text{K}^{-2}$

and  $0.47 \text{ mW}\cdot\text{m}^{-1}\cdot\text{K}^{-2}$  for  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  samples, respectively. In most of the thermoelectric materials, the temperature dependence of the power factor shows a peak value in a narrow temperature range (approximately 100 K) [35], leading to a less efficient conversion when large temperature gradients are imposed. In the case of  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  alloys, the extension of the power factor plateau across a wider temperature range (200–300 K) would allow obtaining optimal conversions also when temperature gradients of hundreds of degrees are used.



**Figure 4.** Electrical conductivity (a), Seebeck coefficient (b), and power factor (c) of the  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  alloys. The transport properties of  $\text{Co}_2\text{TiSn}$  are shown as a comparison [14].



### 3.4. Effect of Composition on Electrical Conductivity, Seebeck Coefficient, and Power Factor

In the case of homogeneous solid solutions, the thermoelectric properties can be modulated on the basis of the fraction of the substituting elements. For example, the substitution effects are deeply known for the  $\text{Fe}_2\text{VAl}$  and  $\text{Fe}_2\text{VAl}$ -related FH compounds [36–39]. In fact, it is known that in multi-substituted Fe-based FH alloys, where the V atoms are replaced with isoelectronic elements (Nb and Ta), the thermoelectric performances result generally enhanced. The properties of the  $\text{Fe}_2\text{XZ}$  alloys can then be finely tuned by introducing specific quantities of substituents; therefore, they can be considered highly versatile compounds [37,38]. Thus, the implementation of these strategies on the Co-based FH alloys would be a considerable step forward in the application of this class of materials.

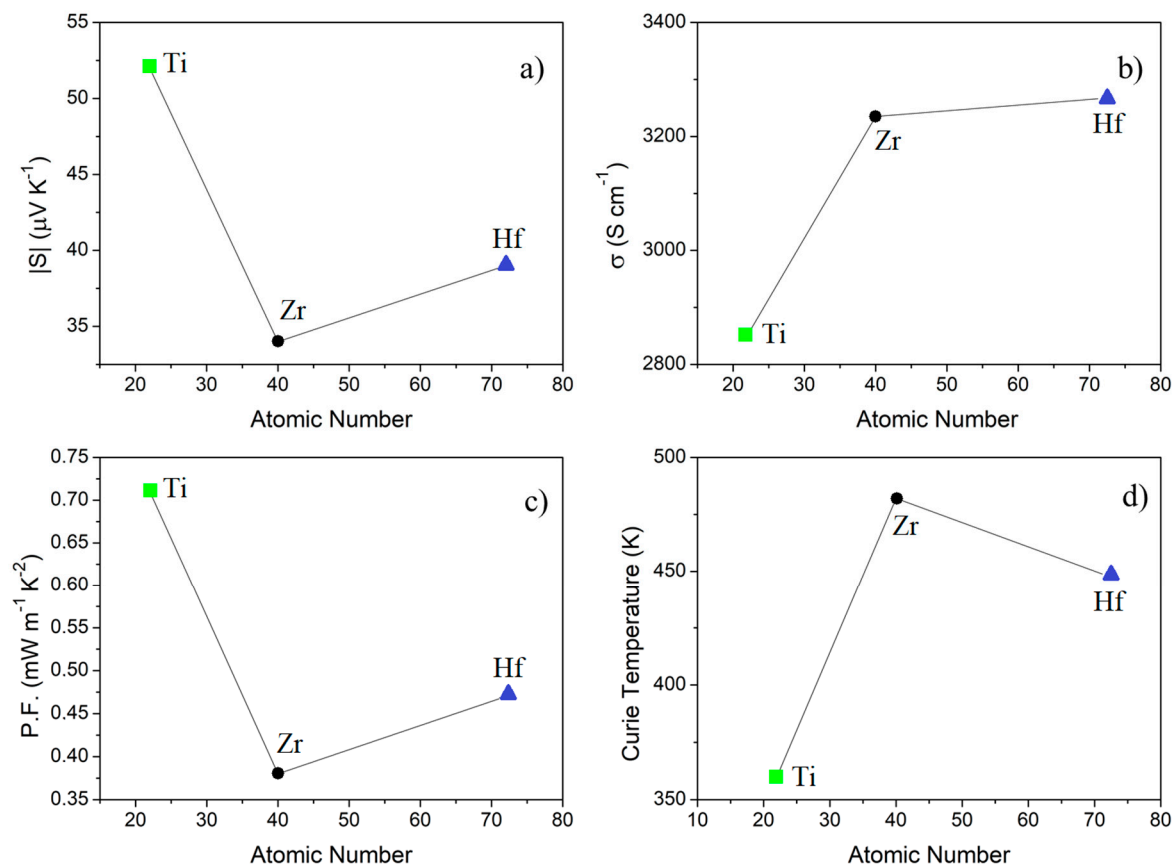
Potentially, isoelectronic substitution of X in  $\text{Co}_2\text{XSn}$  ( $X = \text{Ti, Zr, Hf}$ ) might lead to a complete solubility over the whole compositional range, such as in  $(\text{Zr,Hf})\text{NiSn}$  half-Heusler compound, or to partial solubility in a limited compositional range, such as in  $(\text{Ti,Zr})\text{NiSn}$  and  $(\text{Ti,Hf})\text{NiSn}$  half-Heusler alloys [40].

An overview of the transport properties measured at 673 K for the series of  $\text{Co}_2\text{XSn}$  alloys ( $X = \text{Ti, Zr, Sn}$ ) is reported in Table 3 and they are shown as a function of the atomic number of X in Figure 5. Data for the  $\text{Co}_2\text{TiSn}$  compound have been taken from Ref. [14]. As far as the Seebeck coefficient is concerned,  $\text{Co}_2\text{TiSn}$  shows the highest absolute value of about  $50 \mu\text{V/K}$  after  $T_C$ , while for  $\text{Co}_2\text{HfSn}$  and  $\text{Co}_2\text{ZrSn}$  compounds, values equal to  $38 \mu\text{V/K}$  and  $34 \mu\text{V/K}$ , respectively, can be observed. However, when the electrical conductivity is taken into account,  $\text{Co}_2\text{TiSn}$  is the compound with the lowest  $\sigma$ , while  $\text{Co}_2\text{Hf}$  and  $\text{Co}_2\text{ZrSn}$  display similar values of  $3153 \text{ S/cm}$  and  $3214 \text{ S/cm}$ , respectively. This leads to power factor values of  $0.71 \text{ mW}\cdot\text{m}^{-1}\cdot\text{K}^{-2}$ ,  $0.47 \text{ mW}\cdot\text{m}^{-1}\cdot\text{K}^{-2}$  and  $0.38 \text{ mW}\cdot\text{m}^{-1}\cdot\text{K}^{-2}$  for  $\text{Co}_2\text{TiSn}$ ,  $\text{Co}_2\text{HfSn}$ , and  $\text{Co}_2\text{ZrSn}$  compounds, respectively. All these values are quite high for metallic materials.

**Table 3.** Transport properties and Curie temperature of the  $\text{Co}_2\text{XSn}$  ( $X = \text{Ti, Zr, Sn}$ ) series of full-Heusler alloys. All properties are reported at 673 K.  $T_C$  is the Curie temperature,  $S$  the Seebeck coefficient,  $\sigma$  the electrical conductivity, and PF is the power factor.

Alloy	$T_C$ (K)	$S$ ( $\mu\text{V/K}$ )	$\sigma$ (S/cm)	PF ( $\text{mW}\cdot\text{m}^{-1}\cdot\text{K}^{-2}$ )
$\text{Co}_2\text{TiSn}$ [14]	360	−50	2851	0.71
$\text{Co}_2\text{ZrSn}$	465	−34	3157	0.38
$\text{Co}_2\text{HfSn}$	426	−38	3214	0.47

Considering  $\text{Co}_2\text{TiSn}$  and  $\text{Co}_2\text{HfSn}$ , which respectively show the largest Seebeck coefficient and electrical conductivity in the series, as end members, we could expect that if Ti is progressively substituted by Hf, the absolute value of the Seebeck coefficient would decrease, while the electrical conductivity would increase. As suggested by Figure 5d, the substitution of Ti with Hf would shift the Curie temperature at higher values, similarly to  $\text{Co}_2\text{TiZ}$  ( $Z = \text{Si, Ge, Sn}$ ), where a fine tuning of  $T_C$  can be achieved by substituting the Z atom [14]. An increasing value of  $T_C$  can be useful in spintronics and spin-caloritronics applications, where it is desirable to have ferromagnetic materials even at high temperatures [10].



**Figure 5.** Trends of the transport properties (a): Seebeck coefficient; (b): electrical conductivity; (c): power factor) at 673 K, and Curie temperatures (d) of the  $\text{Co}_2\text{XSn}$  ( $X = \text{Ti, Zr, Hf}$ ) series of full-Heusler alloys as a function of the atomic number of the X element.

#### 4. Conclusions

In this work, the  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  full-Heusler compounds were synthesized by arc melting and characterized from the structural and microstructural point of view. Vickers indentation allowed measuring the microhardness and deriving the fracture toughness,  $K_{IC}$ . Finally, the Seebeck coefficient and electrical conductivity were measured here for the first time. Both the alloys were obtained with sufficiently high purity as as-cast materials. The almost invariance of the relative abundances of phases after annealing reflects that the equilibrium is reached directly by solidification of the melt. The presence of small quantities of secondary phases, as previously reported by other studies [12], can be explained by the observed slight deviation of the samples from the nominal stoichiometry. The two alloys show high hardness (about 900 HV) and fracture toughness typical of ceramics (about  $2 \text{ MPa}\cdot\text{m}^{1/2}$ ). The transport properties of  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  were measured for the first time. The Seebeck coefficient values are negative for both the alloys across the entire range of temperature explored (i.e., from room temperature up to 778 K), indicating an n-type behavior where electrons are the major charge carriers. For both the alloys, the absolute value of the Seebeck coefficient increases almost linearly between room temperature and the Curie temperature and shows a constant plateau after  $T_C$  instead of the typical peak shape. No sign of hysteresis was shown after thermal cycling, indicating the good thermal stability of the alloys in the considered temperature range. Concerning the electrical conductivities, both the compounds are found to behave similar to metals before  $T_C$ , and similar to semiconductors after  $T_C$ ; furthermore, the values of  $\sigma$  set in almost constant plateaus at temperatures sufficiently higher than the Curie point. The power factor of the alloys also exhibits a quite linear increase, followed by a constant ceiling, reflecting the trends of the Seebeck coefficients that are the dominant contributors to the power factor. Taking into account the information available in the

literature for the  $\text{Co}_2\text{TiSn}$  compound, we ordered the transport properties of the  $\text{Co}_2\text{XSn}$  ( $\text{X} = \text{Ti, Zr, Hf}$ ) family of full-Heusler compounds. While  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  show larger electrical conductivities,  $\text{Co}_2\text{TiSn}$  shows a larger absolute value of the Seebeck coefficient. Thus,  $\text{Co}_2\text{TiSn}$  shows the largest power factor in the series. The possible effects of the substitution of Ti with Hf on the electronic transport properties were discussed on the basis of the observed experimental trends.

**Supplementary Materials:** The following are available online at <http://www.mdpi.com/2075-4701/10/5/624/s1>, Figure S1: XRD patterns and Rietveld refinements of the  $\text{Co}_2\text{ZrSn}$  and  $\text{Co}_2\text{HfSn}$  as-cast and annealed alloys, Figure S2: Backscattered electrons SEM images of the  $\text{Co}_2\text{ZrSn}$  as-cast and annealed ingots, Figure S3: Backscattered electrons SEM images of the  $\text{Co}_2\text{HfSn}$  as-cast, and annealed alloys.

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