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24 **Cost-effective visual odometry system for vehicle motion control in**
25 **agricultural environments**

26

27 **Abstract**

28 In precision agriculture, innovative cost-effective technologies and new improved solutions, aimed
29 at making operations and processes more reliable, robust and economically viable, are still needed.

30 In this context, robotics and automation play a crucial role, with particular reference to unmanned
31 vehicles for crop monitoring and site-specific operations. However, unstructured and irregular
32 working environments, such as agricultural scenarios, require specific solutions regarding
33 positioning and motion control of autonomous vehicles.

34 In this paper, a reliable and cost-effective monocular visual odometry system, properly calibrated
35 for the localisation and navigation of tracked vehicles on agricultural terrains, is presented. The
36 main contribution of this work is the design and implementation of an enhanced image processing
37 algorithm, based on the cross-correlation approach. It was specifically developed to use a
38 simplified hardware and a low complexity mechanical system, without compromising
39 performance. By providing sub-pixel results, the presented algorithm allows to exploit low
40 resolution images, thus obtaining high accuracy in motion estimation with short computing time.
41 The results, in terms of odometry accuracy and processing time, achieved during the in-field
42 experimentation campaign on several terrains, proved the effectiveness of the proposed method
43 and its fitness for automatic control solutions in precision agriculture applications.

44

45 **Keywords:** Precision agriculture; Visual odometry; Unmanned ground vehicle (UGV); Real- time
46 image processing; Agricultural field robots

47

48 Nomenclature

CEP_{ε_s}	Circular error probable of translation assessment errors [mm]
$d_{i,j}$	Digital number of pixel located at i^{th} row and j^{th} column of image I
$\bar{d}_{u,v}$	Average values of digital numbers within a portion of image I
$[f_x, f_y]$	x and y component of image focal length [pixel]
g_x	Image pixels spatial resolution [mm/pixel]
g_y	Image pixels spatial resolution [mm/pixel]
h_c	Camera height from the ground [mm]
I_k	Acquired grey scale image at time instant t_k
$\ell_{i,j}$	Digital number of pixel located at i^{th} row and j^{th} column of image L
$\bar{\ell}$	Average values of digital numbers within template $T(\vartheta)$
$L_k(\vartheta)$	Image obtained by rotating image I_k by angle ϑ
n_Γ	Distance threshold from γ_M
m	Coefficient to set the threshold values for γ
$N_i \times N_j$	Image size (height x width) [pixel]
$O_k^{\{UGV\}_k}$	Origin of the $\{UGV\}_k$ reference frame at time t_k
p_T	Template size
$p_{i,j}^{\{UGV\}_k}$	Position of pixel $d_{i,j}$ in the reference frame $\{UGV\}_k$ at time t_k [mm]
$p_{\hat{u},\hat{v}}^{\{UGV\}_{k+1}}$	Position of the template $T_k(\hat{\vartheta})$ centre in image I_{k+1} [mm]
$[p_{c,x}, p_{c,y}]^T$	Position coordinates of the camera centre in the $\{UGV\}_k$ reference frame [mm]
$q(u, v, \vartheta)$	Binary function to select a neighbourhood Γ of $\gamma(u, v, \vartheta)$
$R(\cdot)$	Rotation matrix
$s(\cdot)$ (or $s_k^{k+1}(\cdot)$)	Evaluated vehicle translation (between time instant t_k and t_{k+1}) [mm]
s_r	Reference vehicle translation [mm]
t_k	Generic image acquisition time instant [s]
$T_k(\vartheta)$	Pixel subset, called template, of image $L_k(\vartheta)$
U	Ordered set of u indices
$[\hat{u}_e, \hat{v}_e, \hat{\vartheta}_e]$	Weighted centroid of Γ
$\{UGV\}_k$	Reference frame of the UGV at time t_k
V	Ordered set of v indices
w_T	Semi-width of the template T_k [pixels]
<i>Greek letters</i>	
$\gamma(u, v, \vartheta)$	Normalised cross-correlation function
γ_M	Maximum value of $\gamma(u, v, \vartheta)$
δ_ϑ	Angular resolution of the VO process [deg]
Γ	Specific subset of γ

ε_s	Error in translation assessment between two successive images [mm]
ε_θ	Error in orientation assessment between two successive images [deg]
ϑ	Rotation angle of image $L_k(\vartheta)$ [deg]
$\hat{\vartheta}$	Evaluated vehicle rotation [deg]
ϑ_r	Reference vehicle rotation [deg]
ϑ_{\min}	Minimum value of $\vartheta \in \Theta$ [deg]
ϑ_{\max}	Maximum value of $\vartheta \in \Theta$ [deg]
Θ	Ordered set of all considered rotation angles ϑ ($\Theta = \{\vartheta_{\min}, \vartheta_{\min} + \delta_\theta, \dots, \vartheta_{\max}\}$) [deg]
μ_{ε_θ}	Average of rotation assessment errors [deg]
σ_{ε_s}	Standard deviation of translation assessment errors [mm]
$\sigma_{\varepsilon_\theta}$	Standard deviation of rotation assessment errors [deg]

Acronyms

CCD	Charged coupled device
CEP	Circular error probable
GPS	Global positioning system
GSD	Ground sample distance
IMU	Inertial measurement unit
NCC	Normalised cross correlation
PA	Precision agriculture
SSD	Sum of squared differences
UGV	Unmanned ground vehicle
VO	Visual odometry

49

50 **1. Introduction**

51 Precision agriculture (PA) has been recognised as an essential approach to optimise crop-managing
52 practices and to improve field products quality ensuring, at the same time, environmental safety
53 (Ding et al., 2018; Grella et al., 2017; Lindblom et al., 2017). In very large fields and/or in-fields
54 located on hilly areas, cropland monitoring and maintenance may result in a laborious task,
55 requiring automatic machines and procedures (Comba et al., 2018; Grimstad et al., 2017). In this
56 regard, unmanned ground vehicles (UGVs) are playing a crucial role in increasing efficiency in
57 cultivation, e.g. in optimising the use of fertilisers or precision weed control (Utstumo et al., 2018;
58 Vakilian and Massah, 2017; De Baerdemaeker, 2013).

59 To perform agricultural in-field tasks with the least amount of human interaction, UGVs should
60 be characterised by a high level of automation (van Henten et al., 2013; Kassler, 2001). Nowadays,
61 developed autonomous navigation systems, which use GPS technologies (Bonadies and Gadsden,
62 2018) and/or machine vision approaches (García-Santillán et al., 2017), allow UGVs, for example,
63 to follow crop rows autonomously, even in complex agricultural scenarios. A common
64 requirement for these applications is a robust up-to-date position and orientation assessment during
65 movements (Ghaleb et al., 2017). Despite the wide diffusion of GPS systems, they show
66 limitations and drawbacks when high precision navigation is required or where the satellite signal
67 is poor, e.g. in covered areas, greenhouses or peculiar hilly regions (Ericson and Åstrand, 2018;
68 Aboelmagd et al., 2013). In agricultural environments, UGV motion estimation by wheel odometry
69 also encounters critical limitations due to wheels slippage on sloped terrains, which is very typical
70 in some crops such as vineyards (Bechar and Vigneault, 2016; Aboelmagd et al., 2013; Nourani-
71 Vatani et al., 2009).

72 Visual odometry (VO), the measurement of the position and orientation of a system by exploiting
73 the information provided by a set of successive images (Moravec, 1980), can provide reliable
74 movement feedback in UGV motion control (Aqel et al., 2016; Scaramuzza and Fraundorfer,
75 2011). The hardware required to implement a VO system consists of one or more digital cameras,
76 an image processing unit and an optional lighting system. Not requiring external signals or
77 references, visual odometry has been proven to be very significant in particular contexts where the
78 GPS signal is weak or absent (even where the magnetic field cannot be exploited by compass), by
79 overcoming the limitations of other methodologies (Scaramuzza and Fraundorfer, 2011).

80 Two main typologies of VO systems can be defined on the basis of the adopted number of cameras:
81 (1) stereo systems use data provided by multiple cameras while (2) monocular systems,
82 characterised by a simple and cost-effective setup, exploit a single digital camera. The image
83 processing of stereo systems is typically complex and time consuming and requires accurate
84 calibration procedures; indeed, an unsynchronised shutter speed between the stereo cameras can
85 lead to errors in motion estimation (Aqel et al., 2016; Jiang et al., 2014). However, the stereo
86 system degrades to the monocular case when the stereo baseline (the distance between the two
87 cameras) is small compared to the distance of the acquired scene by the cameras (Aqel et al., 2016).
88 The available image processing algorithms for VO applications have two main approaches: (1)
89 feature-based algorithms and (2) appearance-based algorithms. In feature-based VO, specific

90 features/details detected and tracked in the sequence of successive images are exploited
91 (Fraundorfer and Scaramuzza, 2012). Depending on the application, the performance to be
92 achieved and the different approaches in feature selection, several algorithms can be found in
93 literature, such as Libviso (Geiger et al., 2012), Gantry (Jiang et al., 2014) or the Newton-Raphson
94 search methods (Shi and Tomasi, 1994). A different approach is adopted in appearance based-
95 algorithms where successive image frames are searched for changes in appearance by extracting
96 information regarding pixels displacement. The template matching process, which is a widely
97 recognised approach among VO appearance-based solutions, consists in selecting a small portion
98 within a frame (called template) and in comparing it with a temporally subsequent image, then
99 scoring the quality of the matching (Gonzalez et al., 2012; Goshtasby et al., 1984). This task has
100 mainly been performed by using the sum of squared differences (SSD) and normalised cross-
101 correlation (NCC) as similarity measures (Aqel et al., 2016; Yoo et al., 2014; Nourani-Vatani et
102 al., 2009). This latter matching measure, even if computationally heavier than SSD, is invariant to
103 the linear gradient of image contrast and brightness (Mahmood and Khan, 2012; Lewis, 1995).

104 Motion assessment by VO systems has been proven to be particularly effective when integrated
105 with other sensors such as the inertial measurement unit (IMU), compass sensor, visual compass
106 (Gonzalez et al., 2012), GPS technology or encoders (e.g. on wheels and tracks), to avoid error
107 accumulation on long missions (Zaidner and Shapiro, 2016). Indeed, with particular attention to
108 agricultural applications, innovative and reliable solutions should be developed to reduce system
109 complexity and costs by implementing smart algorithms and by exploiting data fusion (Comba et
110 al., 2016; Zaidner and Shapiro, 2016).

111 In this paper, a reliable and cost-effective monocular visual odometry system, properly calibrated
112 for the localisation and navigation of tracked vehicles on agricultural terrains, is presented. The
113 main contribution of this work is the design and implementation of an enhanced image processing
114 algorithm, based on the cross-correlation approach, with sub-pixel capabilities. It was specifically
115 developed to use a simplified hardware and a low complexity mechanical system, without
116 compromising performance. In the implemented VO system, installed on a full electric tracked
117 UGV, ground images acquisition was performed by an off-the-shelf camera. The performance of
118 the system, in terms of computing time and of movement evaluation accuracy, was investigated
119 with in-field tests on several kinds of terrains, typical of agricultural scenarios. In addition, the

120 optimal set of algorithm parameters was investigated for the specific UGV navigation/motion
121 control for precision agricultural applications.

122 The paper is structured as follows: Section 2 reports the description of the implemented tracked
123 UGV and of the vision system. The proposed algorithm for visual odometry is presented in Section
124 3, while the results from the in-field tests are discussed in Section 4. Section 5 reports the
125 conclusion and future developments.

126

127 **2. System setup**

128 The implemented VO system was developed to perform the motion and positioning controls of a
129 full electric UGV specifically designed for precision spraying in tunnel crop management, where
130 GPS technology is hampered by metal enclosures. Image acquisition is performed by a Logitech
131 C922 webcam, properly positioned in the front part of the vehicle, with a downward looking setup
132 at the height (h_c) of 245 mm from the ground. To improve the quality of the acquired images, the
133 camera was shielded with a properly sized rigid cover to protect the portion of ground within the
134 camera field of view from direct lighting, thus avoiding irregular lighting and the presence of
135 marked shadows. The illumination of the observed ground surface is provided by a lighting system
136 made of 48 SMD LED 5050 modules (surface-mount device light-emitting diode) with an overall
137 lighting power of more than 1,000 lumens and a power consumption of 8.6 W. Fig. 1 reports the
138 diagram of the VO system setup together with an image of the implemented UGV system.

139 The image acquisition campaign was conducted on five different terrains (soil, grass, concrete,
140 asphalt and gravel), typical of agricultural environments, in order to assess and quantify the
141 performance of the proposed algorithm. Two datasets of more than 16,000 pairs of grey scale
142 images (8-bit colour representation), at two image resolutions, were processed. Images with a high-
143 resolution have a size of 1280x720 pixels (width and height) while low-resolution ones, which
144 were obtained by down sampling the high resolution ones, are 320x240 pixels (width and height).
145 The sample images at high and low resolution, acquired on five different terrains, are shown in
146 Fig. 2.

147 A grey scale image I_k , acquired at time instant t_k , can be defined as an ordered set of digital
148 numbers $d_{i,j}$ as

$$I_k = \{d_{i,j} \in [0,1, \dots, 255] \vee 1 \leq i \leq N_i, 1 \leq j \leq N_j\} \quad (1)$$

149 where i and j are the row and column indices while N_i and N_j are the numbers of pixels per row
 150 and column, respectively.

151 The intrinsic camera parameters and acquisition settings were evaluated by performing a
 152 calibration procedure (Matlab[®] calibration toolbox). The focal length in pixel was $(f_x, f_y) =$
 153 $(299.4122, 299.4303)$ and $(f_x, f_y) = (888.5340, 888.8749)$ for the low-resolution and high-
 154 resolution images respectively. The position [mm] of pixels $d_{i,j}$ in the UGV reference frame
 155 $\{UGV\}_k$ at time t_k , defined with origin O_k in the barycentre of the tracked system and with the x-
 156 axis aligned to the vehicle's forward motion direction (Fig. 4), can thus be easily computed as

$$p_{i,j}^{\{UGV\}_k} = \left[\left(j - \left\lfloor \frac{N_j}{2} \right\rfloor \right) \frac{h_c}{f_x}, \left(\left\lfloor \frac{N_i}{2} \right\rfloor - i \right) \frac{h_c}{f_y} \right]^T + [p_{c,x}, p_{c,y}]^T \quad (2)$$

157 where $\frac{h_c}{f_x}$ and $\frac{h_c}{f_y}$ are the pixels' spatial resolutions g_x and g_y [mm/pixel] respectively and $[p_{c,x}, p_{c,y}]^T$
 158 are the position coordinates of the camera centre [mm] in the $\{UGV\}_k$. In the implemented UGV,
 159 the position coordinates of the camera with respect to the barycentre of the tracked system are
 160 $[950, 0]^T$ mm. The relevant camera and images intrinsic parameters adopted in this work are
 161 summarised in Table 1.

162

163 3. Visual odometry algorithms

164 In visual odometry, the objective of measuring the position and orientation of an object at time
 165 t_{k+1} , knowing its position and orientation at time t_k , is performed by evaluating the relative
 166 movement of a solid camera having occurred during time interval $t_{k+1} - t_k$. This task is performed
 167 by comparing the image pair I_k and I_{k+1} , acquired in the ordered time instants t_k and t_{k+1} ,
 168 respectively.

169 In the normalised cross-correlation (NCC) approach, a pixel subset $T_k(\vartheta)$ (also named template)
 170 is selected from the image $L_k(\vartheta)$ centre, which is obtained rotating image I_k by an angle ϑ , as

$$T_k(\vartheta) = \left\{ \ell_{i,j} \in L_k(\vartheta) \mid \left| i - \left\lfloor \frac{N_i}{2} \right\rfloor \right| \leq w_T, \left| j - \left\lfloor \frac{N_j}{2} \right\rfloor \right| \leq w_T \right\} \quad (3)$$

171 where $\ell_{i,j}$ is a digital number of image L_k and w_T is the semi-width [pixels] of the template T_k .

172 The adopted template size p_T can be defined as a fraction of the shortest image dimension as $p_T =$
 173 $2 \cdot w_T \cdot N_i^{-1}$; with this definition $p_T \subset [0, 1]$. With no assumption on the performed movement,
 174 angle ϑ is usually selected from an ordered set of values $\Theta = \{\vartheta_{\min}, \vartheta_{\min} + \delta_\vartheta, \dots, \vartheta_{\max}\}$, with

175 ϑ_{\min} and ϑ_{\max} chosen to consider the whole circle angle. The δ_{ϑ} parameter can be defined as the
 176 angular resolution of the process.

177 The relative movement of I_{k+1} with respect to image I_k , in terms of translation $[\hat{u}, \hat{v}]^T$ [pixels] and
 178 rotation $\hat{\vartheta}$ [deg], is thus performed by assessing the position of the ground portions represented in
 179 templates $T_k(\vartheta)$ in the subsequent image I_{k+1} by solving the problem

$$\gamma_M = \max_{\hat{u}, \hat{v}, \hat{\vartheta}} \gamma(u, v, \vartheta) \quad (4)$$

180 with $u \in U = \{w_T, w_T + 1, \dots, N_i - w_T\}$, $v \in V = \{w_T, w_T + 1, \dots, N_j - w_T\}$, $\vartheta \in \Theta$ and where
 181 $\gamma(u, v, \vartheta)$ is the normalised cross-correlation function (Aqel et al., 2016; Lewis, 1995) defined as

$$\gamma(u, v, \vartheta) = \frac{\sum_{i=-w_T}^{w_T} \sum_{j=-w_T}^{w_T} (d_{i+u, j+v} - \bar{d}_{u, v})_{I_{k+1}} \cdot (\ell_{i+w_T, j+w_T} - \bar{\ell})_{T_k(\vartheta)}}{\sqrt{\sum_{i=-w_T}^{w_T} \sum_{j=-w_T}^{w_T} (d_{i+u, j+v} - \bar{d})_{I_{k+1}}^2 \cdot (\ell_{i+w_T, j+w_T} - \bar{\ell})_{T_k(\vartheta)}^2}} \quad (5)$$

182 with

$$\bar{d}_{u, v} = \frac{\sum_{i=-w_T}^{w_T} \sum_{j=-w_T}^{w_T} (d_{i+u, j+v})_{I_{k+1}}}{4 \cdot w_T^2} \quad (6)$$

183 and

$$\bar{\ell} = \frac{\sum_{i=-w_T}^{w_T} \sum_{j=-w_T}^{w_T} (\ell_{i+w_T, j+w_T})_{T_k(\vartheta)}}{4 \cdot w_T^2} \quad (7)$$

184 the average values of the digital numbers within a portion of image I_{k+1} and template $T_k(\vartheta)$,
 185 respectively. A scheme of the implemented NCC algorithm is reported in Fig. 3.

186 The relative movement s_k^{k+1} performed by the UGV in the time interval $t_{k+1} - t_k$ (Fig. 4) can thus
 187 be easily computed as

$$s_k^{k+1}(\hat{u}, \hat{v}, \hat{\vartheta}) = R(-\hat{\vartheta}) \cdot p_{\hat{u}, \hat{v}}^{\{UGV\}_{k+1}} - p_{\left[\frac{N_i}{2}, \left|\frac{N_j}{2}\right|\right]}^{\{UGV\}_k} \quad (8)$$

188 where $R(-\hat{\vartheta})$ is the rotation matrix of angle $-\hat{\vartheta}$, $p_{\hat{u}, \hat{v}}^{\{UGV\}_{k+1}}$ is the template $T_k(\hat{\vartheta})$ assessed position
 189 [mm] in I_{k+1} (represented in $\{UGV\}_{k+1}$, Eq. (2)), and $p_{\left[\frac{N_i}{2}, \left|\frac{N_j}{2}\right|\right]}^{\{UGV\}_k}$ is the known position [mm] of

190 template T_k in I_k , (represented in $\{UGV\}_k$, Eq. (2)). For the sake of clarity, it should be noted that
 191 $p_{\left[\frac{N_i}{2}, \left|\frac{N_j}{2}\right|\right]}^{\{UGV\}_k}$ is equal to $[p_{c,x}, p_{c,y}]^T$, which is $[950, 0]^T$ millimetres, and that $s_k^{k+1}(\hat{u}, \hat{v}, \hat{\vartheta})$ coincides

192 with $O_{k+1}^{\{UGV\}_k}$, which is the origin of the reference frame $\{UGV\}_{k+1}$ represented in $\{UGV\}_k$
193 reference frame (Fig. 4).

194

195 **3.1 Enhanced cross-correlation algorithm**

196 The quality of the UGV's movement measure, using normalised cross-correlation-based visual
197 odometry algorithms, is strictly related to the solution of the problem defined in Eq. (4). The
198 approach of considering the sole maximum value γ_M of $\gamma(u, v, \vartheta)$, with $u \in \{w_T, w_T + 1, \dots, N_i -$
199 $w_T\}$, $v \in \{w_T, w_T + 1, \dots, N_j - w_T\}$ and $\vartheta \in \Theta$, has intrinsic limitations regarding maximum
200 achievable accuracy. Indeed, the digital discretisation of the field of view performed by the digital
201 camera and the discrete set Θ of the investigated orientation ϑ affect both the translation and the
202 rotation assessments. The accuracy of the VO system is thus related to the adopted image
203 resolution, being directly related to the pixels ground sample distance (GSD) g_x and g_y and the
204 angle step δ_ϑ adopted in the image processing. Regarding this aspect, an accuracy improvement
205 can be pursued by adopting high-resolution cameras, which can provide images with smaller pixels
206 GSD g_x and g_y : favourable effects are linked, in the meanwhile, to the accuracy of $[\hat{u}, \hat{v}]^T$ and to
207 the angular resolution δ_ϑ values. Indeed, concerning the rotation procedure of image $L_k(\delta_\vartheta)$, if the
208 rotation angle δ_ϑ is small, no modifications are obtained on the pixels' digital number in the central
209 part of the image, where the template is selected. For the sake of clarity, the smallest δ_ϑ values
210 which lead to template $T_k(\delta_\vartheta)$ modifications, in relation to image resolution and template size p_T ,
211 are reported in Table 2.

212 However, increasing image resolution leads to a considerable increment in the required computing
213 load, which does not fit with the real-time requirements of the VO algorithm application or requires
214 technologies which are too expensive.

215 The proposed approach is aimed at increasing VO assessment accuracy by using very low-
216 resolution images, which allows to drastically reduce the computing load while achieving results
217 comparable to the ones obtained by processing high-resolution data. This translates into more cost-
218 effective systems, requiring economical acquisition and processing hardware.

219 For this purpose, a function $q(u, v, \vartheta)$ was defined as

$$\begin{aligned}
& q(u, v, \vartheta) \\
& = \begin{cases} 0 & \text{if } \gamma(u, v, \vartheta) < m \cdot \gamma_M, \quad \left\| ([u, v, \vartheta] - [\hat{u}, \hat{v}, \hat{\vartheta}]) \circ [1, 1, \delta_\vartheta^{-1}] \right\|_2 > n_\Gamma \\ 1 & \text{if } \gamma(u, v, \vartheta) \geq m \cdot \gamma_M, \quad \left\| ([u, v, \vartheta] - [\hat{u}, \hat{v}, \hat{\vartheta}]) \circ [1, 1, \delta_\vartheta^{-1}] \right\|_2 \leq n_\Gamma \end{cases} \quad (9)
\end{aligned}$$

220 in order to consider a neighbourhood Γ of the maximum γ_M (Eq. (4)) of cross-correlation discrete
221 function $\gamma(u, v, \vartheta)$ in the space (u, v, ϑ) , with values higher than $m \cdot \gamma_M$. In particular, n_Γ is the
222 distance threshold from γ_M and m is the coefficient to set the γ values threshold. In this work,
223 adopted values are $n_\Gamma = 5$ and $m = 0.95$ on the base of empirical evaluations. The Hadamard
224 product with $[1, 1, \delta_\vartheta^{-1}]$ was adopted to normalise the weight of the three spatial coordinates
225 (u, v, ϑ) .

226 The enhanced movement assessment is thus performed by computing the weighted centroids
227 $[\hat{u}_e, \hat{v}_e, \hat{\vartheta}_e]$ of Γ (Fig. 5), as

$$\hat{u}_e = \frac{\sum_{u=w_T}^{N_i-w_T} u \cdot \sum_{v=w_T}^{N_j-w_T} \sum_{z=1}^{\text{card}(\Theta)} \gamma(u, v, \vartheta_z) \cdot q(u, v, \vartheta_z)}{\sum_{u=w_T}^{N_i-w_T} \sum_{v=w_T}^{N_j-w_T} \sum_{z=1}^{\text{card}(\Theta)} q(u, v, \vartheta_z)} \quad (10)$$

228

$$\hat{v}_e = \frac{\sum_{v=w_T}^{N_j-w_T} v \cdot \sum_{u=1}^{N_i-w_T} \sum_{z=1}^{\text{card}(\Theta)} \gamma(u, v, \vartheta_z) \cdot q(u, v, \vartheta_z)}{\sum_{u=w_T}^{N_i-w_T} \sum_{v=w_T}^{N_j-w_T} \sum_{z=1}^{\text{card}(\Theta)} q(u, v, \vartheta_z)} \quad (11)$$

229 and

$$\hat{\vartheta}_e = \frac{\sum_{z=1}^{\text{card}(\Theta)} z \cdot \sum_{u=w_T}^{N_i-w_T} \sum_{v=w_T}^{N_j-w_T} \gamma(u, v, \vartheta_z) \cdot q(u, v, \vartheta_z)}{\sum_{u=w_T}^{N_i-w_T} \sum_{v=w_T}^{N_j-w_T} \sum_{z=1}^{\text{card}(\Theta)} q(u, v, \vartheta_z)} \quad (12)$$

230 With the proposed approach, the UGV's movement evaluation is not defined by discrete values,
231 since $[\hat{u}_e, \hat{v}_e, \hat{\vartheta}_e] \in \mathbb{R}^3$.

232

233 4. Results and discussion

234 The performance of the proposed visual odometry system, developed for a UGV motion
235 estimation, was assessed by processing more than 16,000 images. The in-field tests were
236 performed on different agricultural terrains by acquiring images on soil, grass, asphalt, concrete
237 and gravel. In particular, both rectilinear and curvilinear paths were planned. Considering the
238 whole dataset, the travelled distance between two subsequent images ranges between 0 mm (static
239 vehicle) and 70 mm, which guarantees a minimum overlapping area of 72%. The relative rotation

240 does not exceed the range of $[-9 +9]$ degrees, due to the short movement between two acquired
 241 frames. The image resolutions were 1280×720 pixels (high-resolution images) and 320×240 pixels
 242 (low-resolution images). To evaluate the performance improvements of the proposed algorithm,
 243 with sub-pixel capabilities, the set of acquired images was also processed by means of a standard
 244 VO algorithm (Computer Vision System Toolbox, MathWorks, 2018).

245 The performance analysis of the proposed VO system was performed: (1) by assessing motion
 246 evaluation accuracy in pairs of successive images, using high-resolution datasets as a reference,
 247 and (2) by computing the cumulative error with respect to in-field position references travelling
 248 about 10 meters long paths.

249 Concerning a pair of successive images, the error in measuring the relative movement s and the
 250 rotation ϑ between two subsequent images was defined as

$$\varepsilon_s = \|s(\cdot) - s_r\|_2 \quad (13)$$

251 and

$$\varepsilon_\vartheta = |\hat{\vartheta} - \vartheta_r| \quad (14)$$

252 respectively, where $s(\cdot)$ (Eq. (8)) and $\hat{\vartheta}$ are the vehicle's movement and rotation, evaluated by
 253 using the enhanced and standard algorithm and by processing low-resolution images, while s_r and
 254 ϑ_r represent the reference measurements from the high-resolution images. Concerning the
 255 translation assessment, accuracy was expressed by the circular error probable (CEP_{ε_s}) and standard
 256 deviation (σ_{ε_s}) indices (Winkler et al., 2012) (Table 3), while accuracy in measuring the changes
 257 in vehicle orientation ϑ were described by computing the average ($\mu_{\varepsilon_\vartheta}$) and standard deviation
 258 ($\sigma_{\varepsilon_\vartheta}$) of the computed ε_ϑ errors (Table 4). The results were detailed for each in-field test performed
 259 on a specific kind of terrain and, finally, computed by considering the whole image dataset. Overall
 260 accuracy in the translation assessment of the proposed algorithm across different terrains resulted
 261 to be $CEP_{\varepsilon_s} = 0.16$ mm, with an improvement of around 54% with respect to the values obtained
 262 by processing the images with the standard algorithm, which shows a CEP_{ε_s} of 0.37 mm. The
 263 average error in the vehicle's orientation assessment was $\mu_{\varepsilon_\vartheta} = 0.26$ degrees, with an
 264 improvement of around 67.6% with respect to the values obtained by processing the images with
 265 the standard algorithm. The typology of terrain slightly affects the achieved performance: on the
 266 grass surface, a lower performance improvement was found compared to other terrains. Indeed,
 267 the greater variability in object height within the camera field of view can lead to additional

268 perspective errors. Nevertheless, even in these complex scenarios, improvements of 44% in the
269 CEP_{ε_s} and of 34% in the orientation assessment was observed ($CEP_{\varepsilon_s} = 0.19$ mm and $\mu_{\varepsilon_\theta} = 0.42$
270 degree) compared to the ones obtained by the standard algorithm. Boxplots of errors ε_s and ε_θ ,
271 computed by considering the whole image dataset, are reported in Fig. 6 for standard and enhanced
272 algorithms. The x and y components of ε_s and the CEP_{ε_s} circles are detailed in Fig. 7, with ε_θ
273 represented by using a colour bar.

274 The cumulative error was computed for 20 sample paths of the tracked vehicle with a length of 9.6
275 meters, defined as a curvilinear path generated by a sinusoidal trajectory of 0.15 m amplitude and
276 of 3.2 m period. The number of acquired images for a path repetition ranges between 156 and 166,
277 with an average travelled distance between two consecutive frames of 61 mm. Defining a
278 normalised cumulative error with respect to the travelled distance, the obtained values are 0.08
279 and 0.84 [$\text{deg} \cdot \text{m}^{-1}$] for what concerns translation and orientation, respectively. The improvement
280 compared to the standard algorithm is of about 60% for both the translation and orientation
281 assessments. The boxplots of all the obtained cumulative errors, expressed in normalised values,
282 are reported in Fig. 8. Considering a constant travelled distance, the cumulative error is strictly
283 related to the number of processed images, as every processing step contributes to the overall error.
284 With this assumption, to minimise the cumulative error, pairs of frames acquired at the largest
285 distance, still guaranteeing the proper overlapping surface, should be used. For this purpose, a
286 multi-frame approach can further improve system performance (Jiang et al., 2014).

287 The optimal configuration for a VO system setup requires thorough analysis of the parameters
288 related to image processing and their tuning according to the application requirements. With
289 particular attention to the overall VO system performance, the size p_T of the template $T_k(\vartheta)$ is a
290 relevant algorithm parameter since it is strictly related to (1) the motion accuracy measure, (2) the
291 allowed maximum length of the relative movement between two subsequent images, which should
292 still assure the required overlapping surface of the template, (3) the computing time and, thus, (4)
293 the maximum allowed velocity with a specific VO setup.

294 The template size p_T has a non-linear and non-monotonic effect on the overall VO system's
295 accuracy. Considering the translation assessment, by varying p_T within the range 0.05-0.35, an
296 optimal value can be found that provides the best accuracy. Indeed, the proposed algorithm
297 achieves a $CEP_{\varepsilon_s} = 0.16$ mm for $p_T = 0.20$, while accuracy degrades to $CEP_{\varepsilon_s} = 0.21$ mm and
298 $CEP_{\varepsilon_s} = 0.22$ for $p_T = 0.05$ and $p_T = 0.35$, respectively. The boxplots of errors ε_s and ε_θ ,

299 obtained by setting p_T within the range 0.05-0.35, are reported in Figs. 9 and 10, respectively. The
300 observed accuracy trend in determining the vehicle's orientation is similar to the one described for
301 translation, with the exception of the effect of p_T values greater than 0.20 on the accuracy's
302 decrement: it is less marked until p_T exceeds 0.6, values that lead to insufficient overlapping
303 surfaces between two successive images. Indeed, regarding proper overlapping surfaces between
304 successive images, the template size should not exceed a certain value. Larger template sizes p_T
305 require a shorter relative movement of the vehicle between image acquisition time instants to avoid
306 complete mismatch between a pair of successive images. In the implemented VO system
307 performance evaluation, increasing p_T from 0.1 to 0.6 will limit the maximum allowed movement
308 from 93.1 to 39.2 mm, requiring a higher framerate to keep proper image acquisition when
309 considering a constant vehicle velocity.

310 Concerning the computing time, smaller p_T values allow to drastically reduce the required time to
311 process an image pair: considering a low-resolution dataset, the average computing time (0.02
312 seconds) using $p_T = 0.05$ is 88% shorter than the one required by $p_T = 0.35$ (0.19 seconds). Fig.
313 11a reports the average computing time obtained for processing low and high resolution images
314 with a template size p_T ranging from 0.05 to 0.8.

315 Consequently, the allowed maximum velocity of the vehicle is thus strictly related to template
316 size: considering a constant computing power, smaller template sizes lead to higher vehicle
317 maximum speeds, due to the concurrent effects on the processing time required for an image pair
318 and the length of the maximum allowed movement between two subsequent images. In the
319 implemented VO system, processing low-resolution images by using a value of $p_T = 0.05$, the
320 upper limit velocity (about $4.1 \text{ m} \cdot \text{s}^{-1}$) is 91% greater than the one allowed by $p_T = 0.35$ (about
321 $0.3 \text{ m} \cdot \text{s}^{-1}$). The maximum allowed velocities for low and high-resolution images with respect to
322 template size p_T ranging from 0.05 to 0.8 are represented in Fig. 11b.

323

324 **5. Conclusions**

325 In this paper, an enhanced image processing algorithm for a cost-effective monocular visual
326 odometry system, aimed at obtaining highly reliable results at low computational costs for a
327 tracked UGV navigation in agricultural applications, is presented. The implemented VO system
328 consists of a downward looking low cost web-camera sheltered with a rigid cover to acquire
329 images with uniform LED lighting. Based on the normalised cross-correlation methodology, the

330 proposed VO algorithm was developed to exploit low-resolution images (320x240 pixels),
331 achieving sub-pixel accuracy in motion estimation. The algorithm allows the VO system to be
332 applied to real-time applications using cost-effective hardware, by requiring a lower computational
333 load.

334 The robustness of the proposed VO algorithm was evaluated by performing an extensive in-field
335 test campaign on several terrains typical of agricultural scenarios: soil, grass, concrete, asphalt and
336 gravel. The relationship between system performances and more relevant algorithm parameters
337 was investigated in order to determine a proper final system setup.

338 The obtained overall accuracy, in terms of circular probable error and normalised cumulative error,
339 which are 0.16 mm and 0.08 respectively, were compatible with UGV requirements for precision
340 agricultural applications. The obtained short computing time allowed the vehicle to achieve a
341 maximum velocity limit higher than $4 \text{ m} \cdot \text{s}^{-1}$.

342 Based on the relative motion assessment, the performance of VO systems degrades when
343 incrementing path length. Therefore, the system integration with absolute reference is required to
344 maintain the needed accuracy during long mission paths.

345

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351

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